

Constrained Motion Strategies for Robotic Systems

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Advisor: Professor Khatib

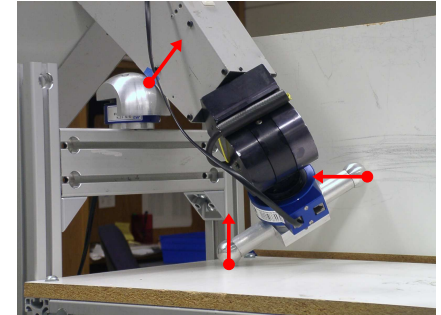
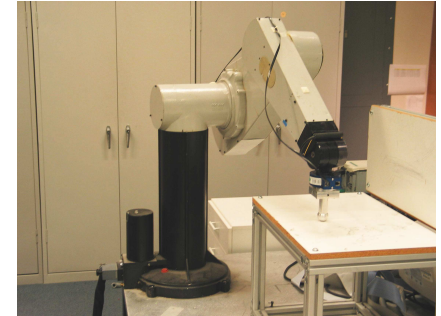
Artificial Intelligence Laboratory

Computer Science Department

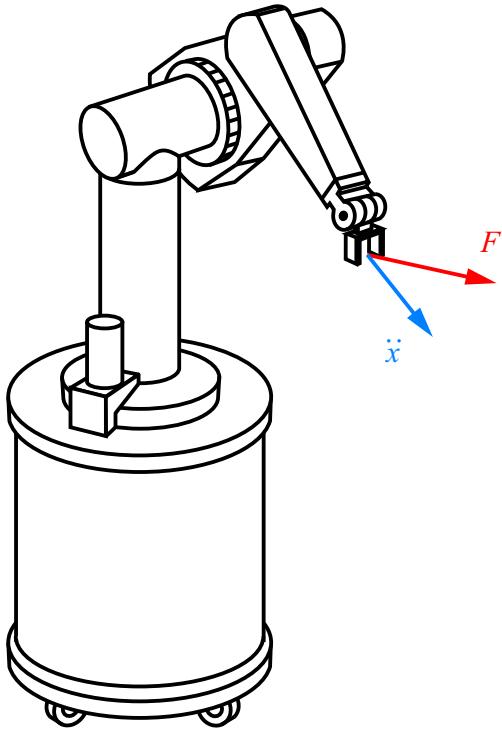
Stanford University

Contributions

- Robust force control for multi-body robotic systems
 - High fidelity haptically augmented teleoperation
- Development of generalized motion/force control structure for multi-link multi-contact
- Contact force consistent motion/force control strategy for humanoid systems



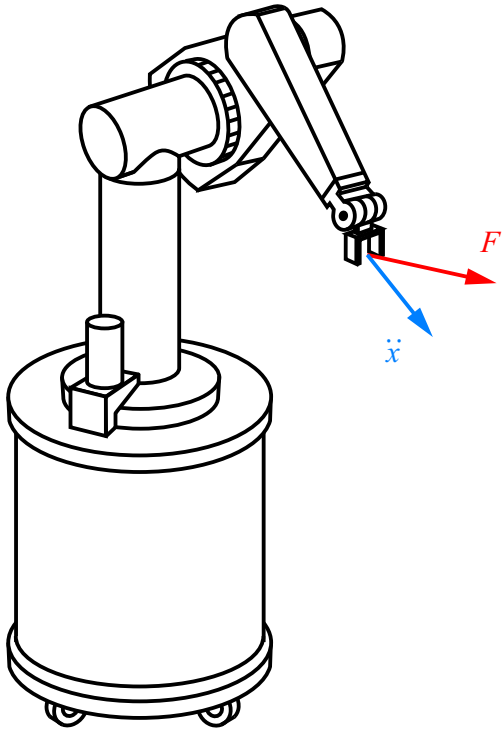
Motion Control



The operational space formulation (Khatib 87)
Equations of motion in joint space

$$A\ddot{q} + b(q, \dot{q}) + g(q) = \Gamma$$

Motion Control



The operational space formulation (Khatib 87)

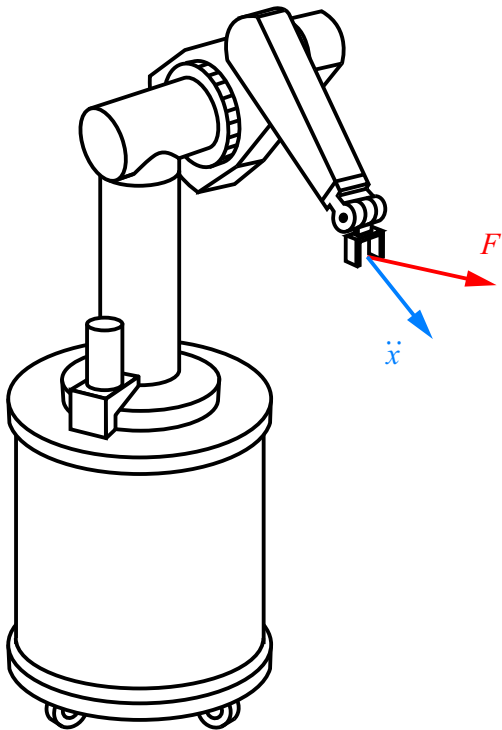
Equations of motion in joint space

$$A\ddot{q} + b(q, \dot{q}) + g(q) = \Gamma$$

Dynamics in the operational space

$$\Lambda\ddot{x} + \mu(q, \dot{q}) + p(q) = F$$

Motion Control



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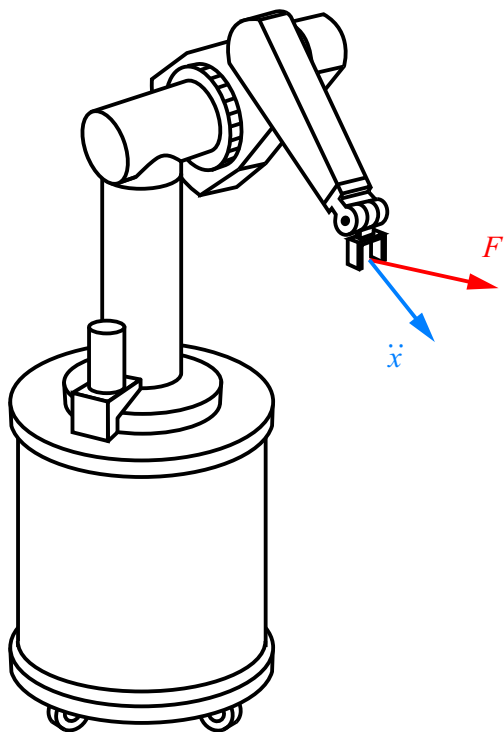
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Control force

$$F = \hat{\Lambda}f^* + \hat{\mu}(q, \dot{q}) + \hat{p}(q)$$

Motion Control



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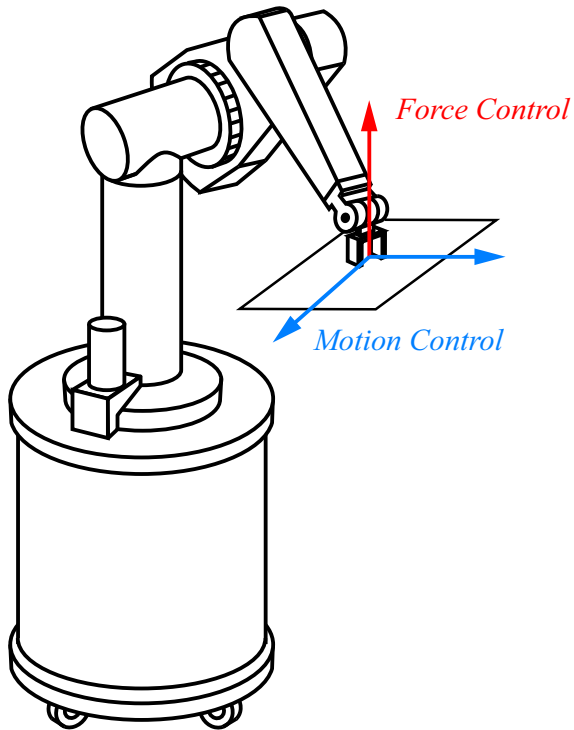
Control force

$$F = \hat{\Lambda}f^* + \hat{\mu}(q, \dot{q}) + \hat{p}(q)$$

The operational space formulation was extended to handle multiple points (Russakow, Khatib, and Rock 1995)

$$x = [x_1, x_2, \dots, x_m]^T$$

Motion/Force Control

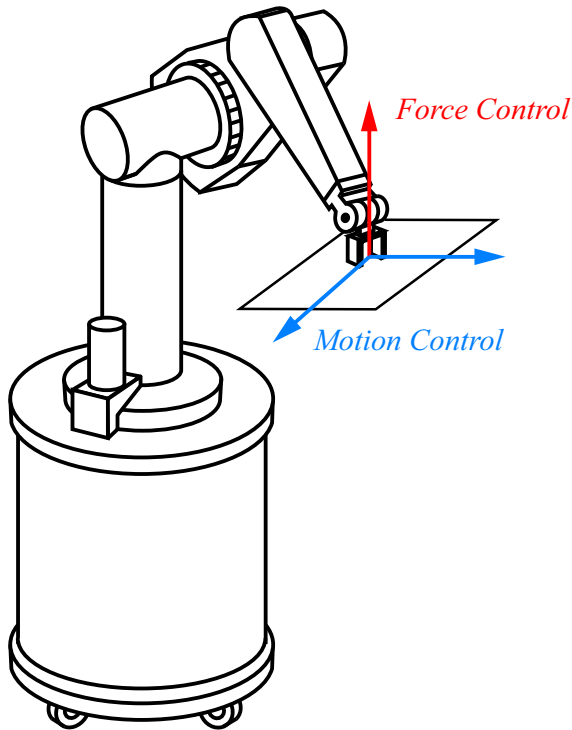


Control force

$$F = \hat{\Lambda} f^* + \hat{\mu}(q, \dot{q}) + \hat{p}(q) + \hat{f}_c$$

Compliant frame selection matrix Ω_f
and Ω_m (Raibert and Craig 81, Khatib
87)

Motion/Force Control



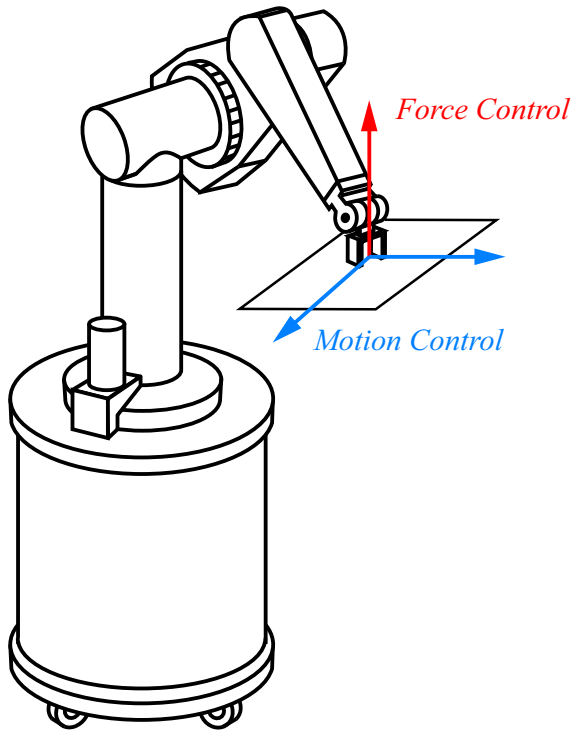
Control force

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Compliant frame selection matrix Ω_f and Ω_m (Raibert and Craig 81, Khatib 87)

$$f^* = \Omega_f f_f^* + \Omega_m f_m^*$$

Motion/Force Control



Control force

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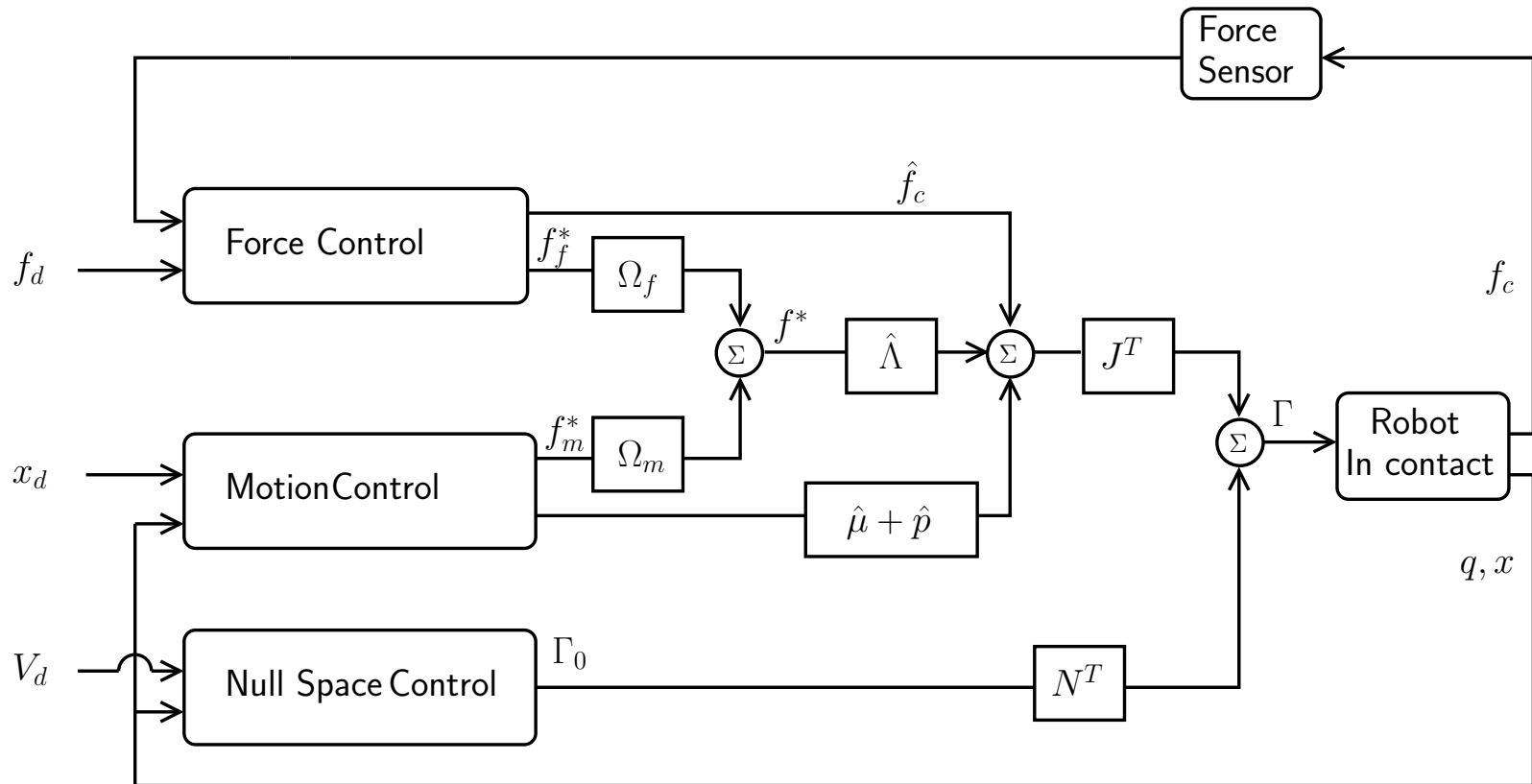
Compliant frame selection matrix Ω_f and Ω_m (Raibert and Craig 81, Khatib 87)

$$f^* = \Omega_f f_f^* + \Omega_m f_m^*$$

With environmental model (stiffness k_s),

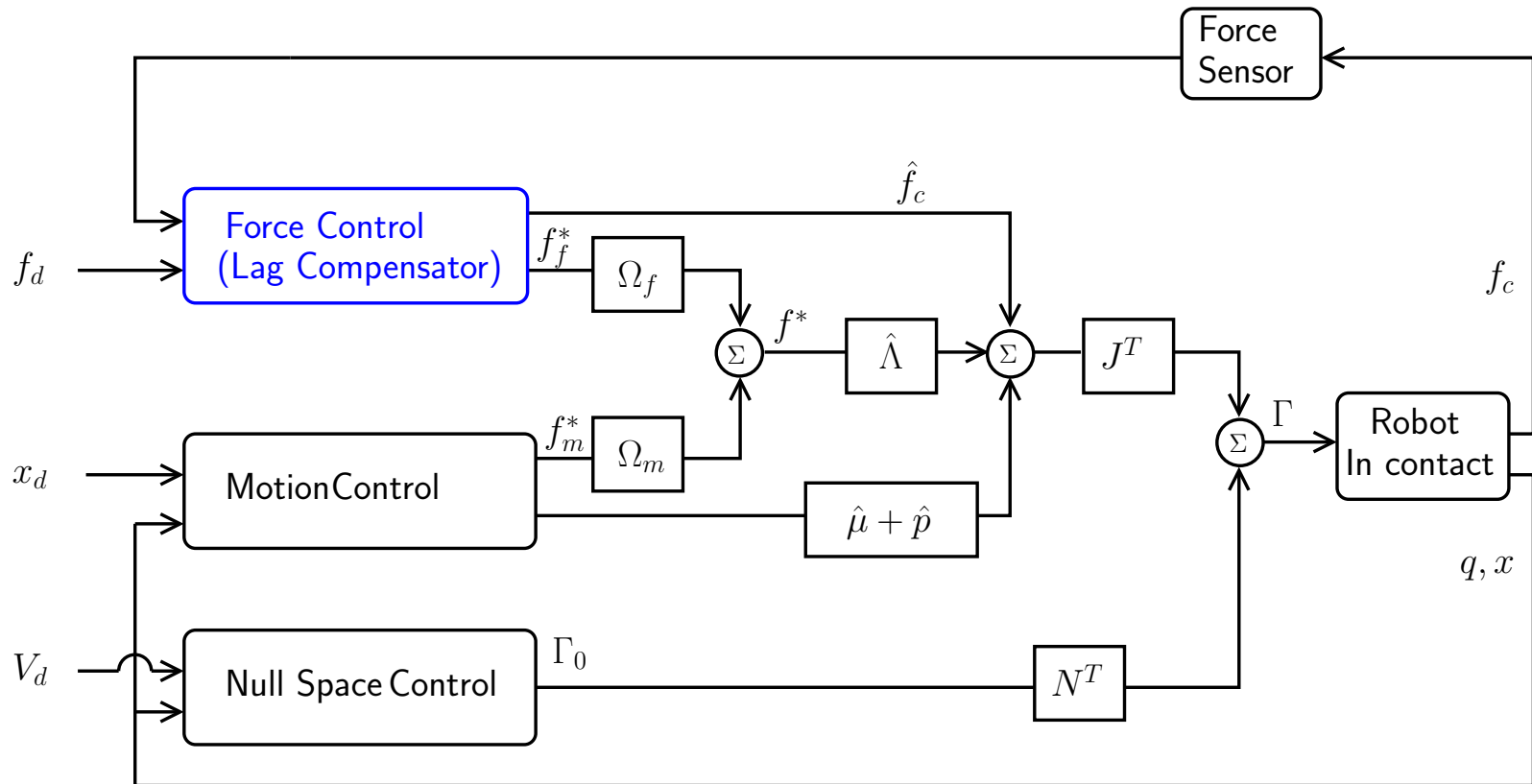
$$\begin{cases} \ddot{x}_m &= f_m^* \\ \frac{1}{k_s} \ddot{f}_c &= f_f^* \end{cases}$$

Motion/Force Control Framework



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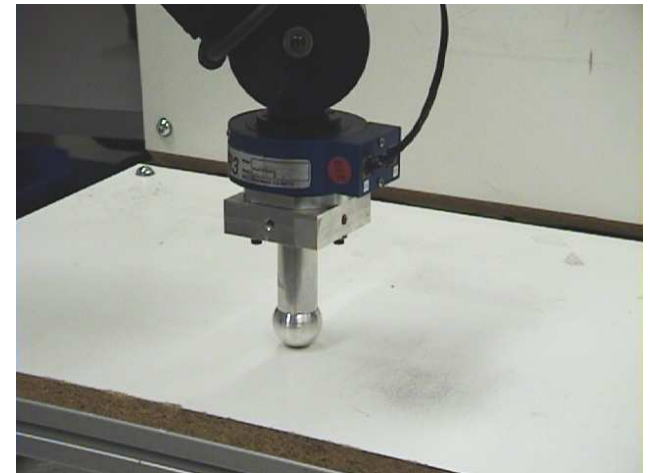
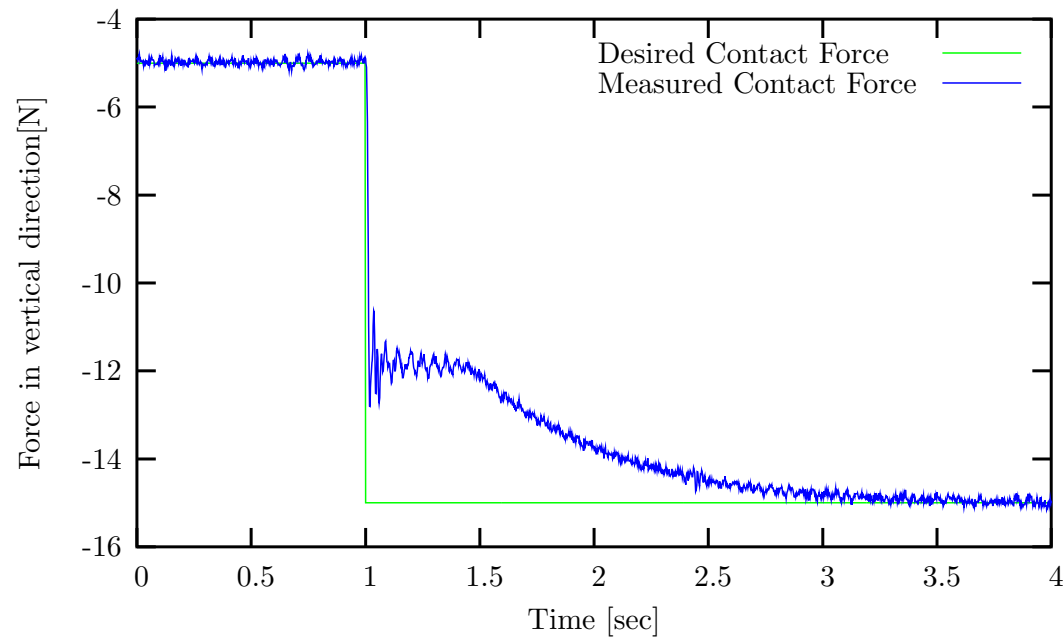
Motion/Force Control Framework



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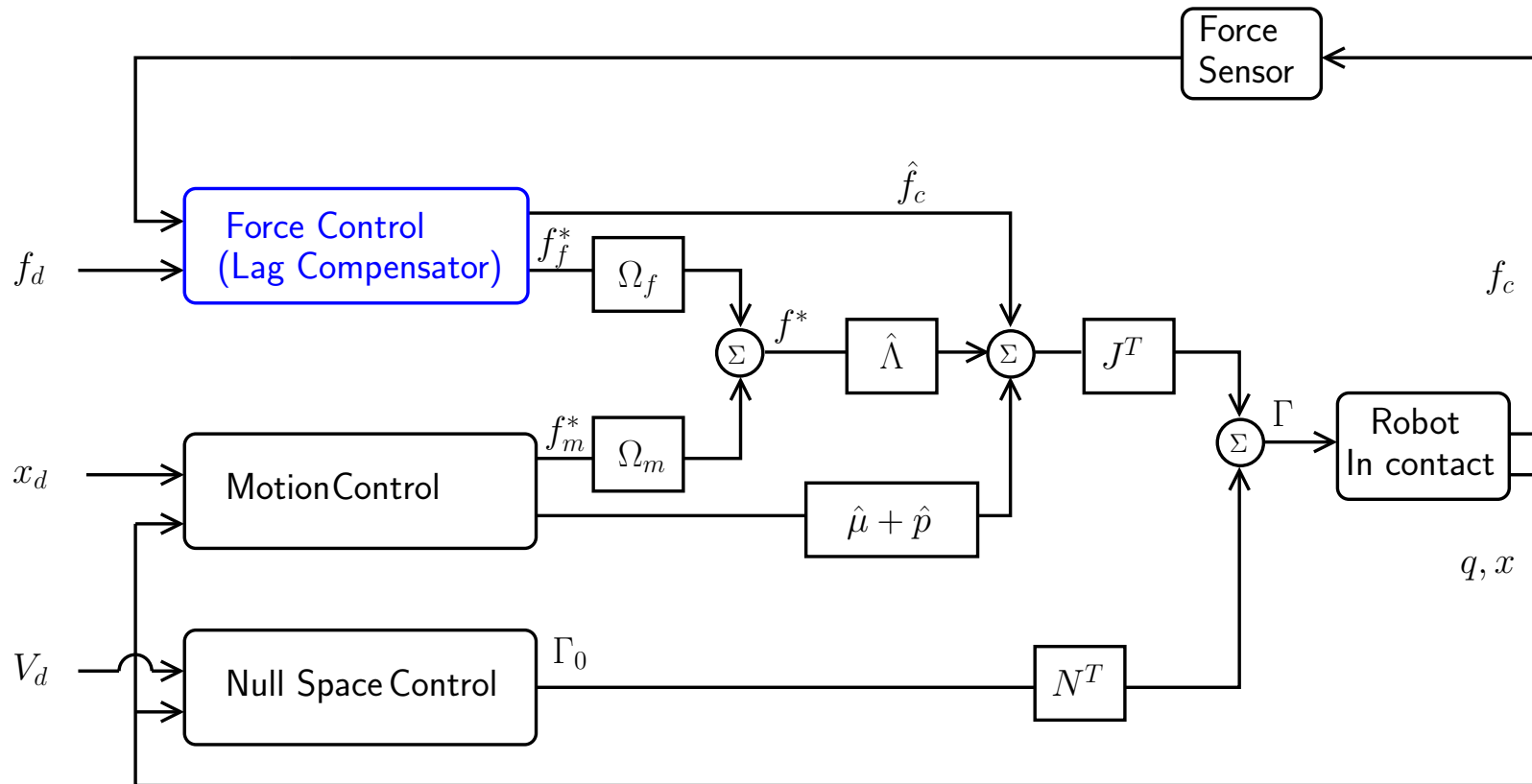
Force Control Result

One point contact with hard surface



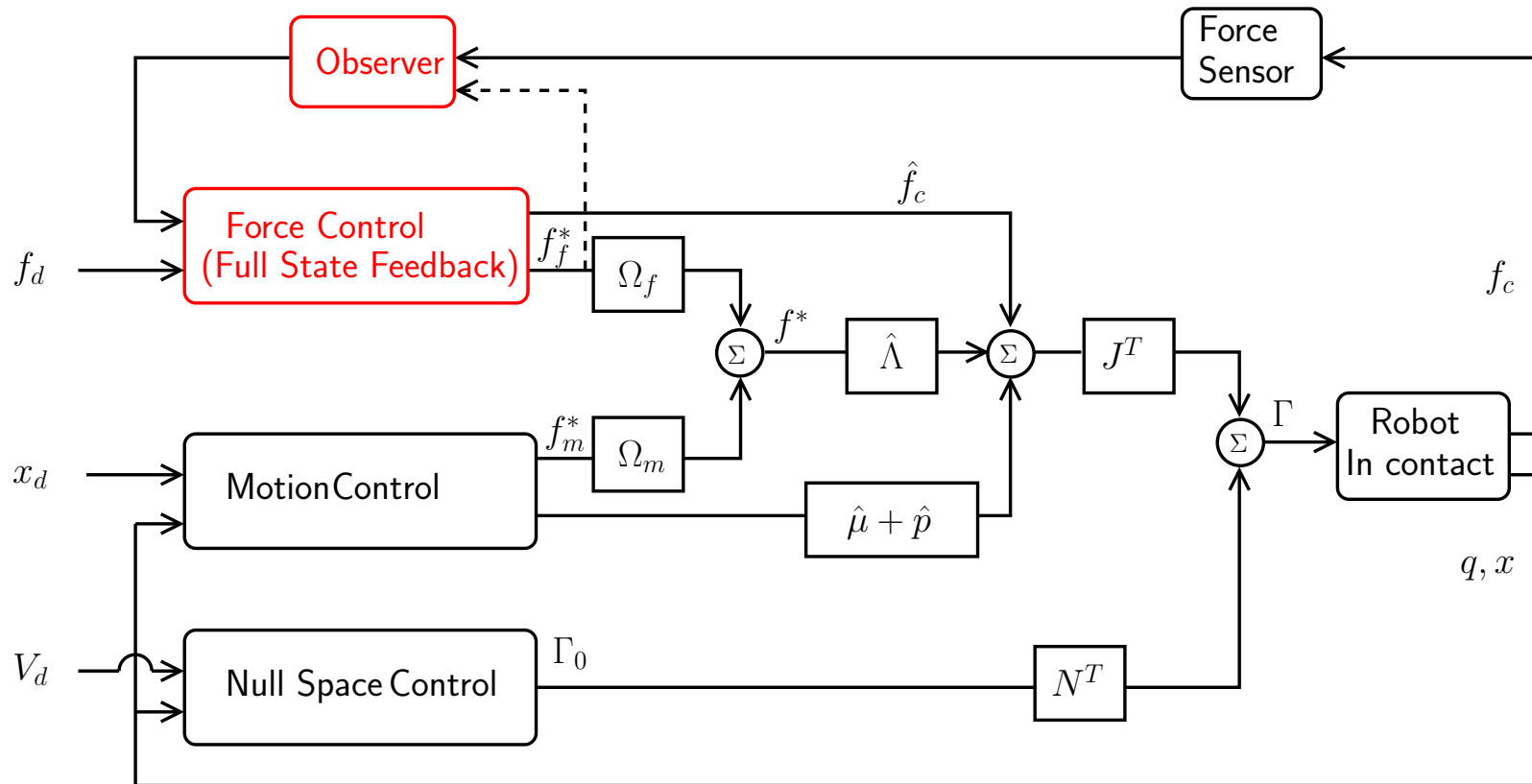
Lag compensator

Motion/Force Control Framework



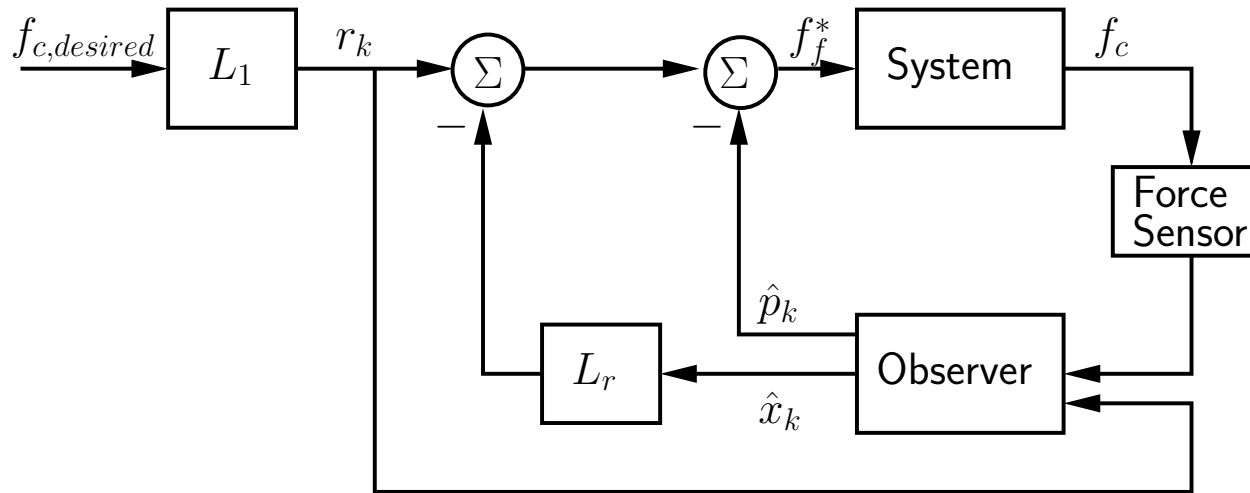
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Motion/Force Control Framework



$$\begin{cases} \ddot{x}_m = f_m^* \\ \frac{1}{k_s} \ddot{f}_c = f_f^* \end{cases}$$

Control with Estimator



\hat{x}_k state estimate - \hat{f}_c and $\hat{\dot{f}}_c$

\hat{p}_k input disturbance estimate

L_r a full state feedback gain obtained by Pole Placement Method

L_1 a scaling factor to compute reference input

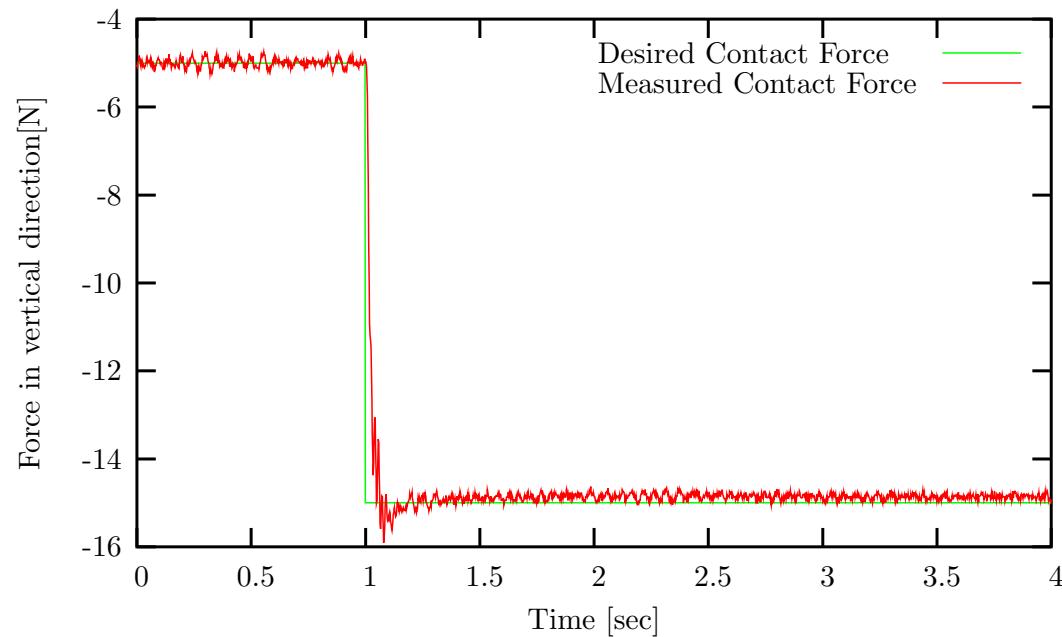
f_c contact force

$f_{c,d}$ desired contact force

r_k reference input

Force Control Result

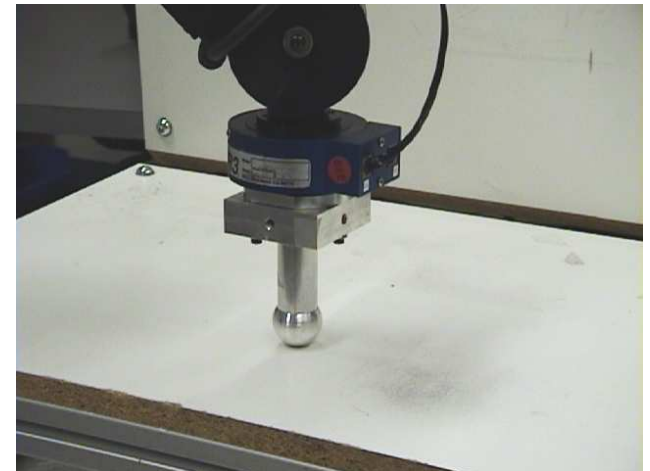
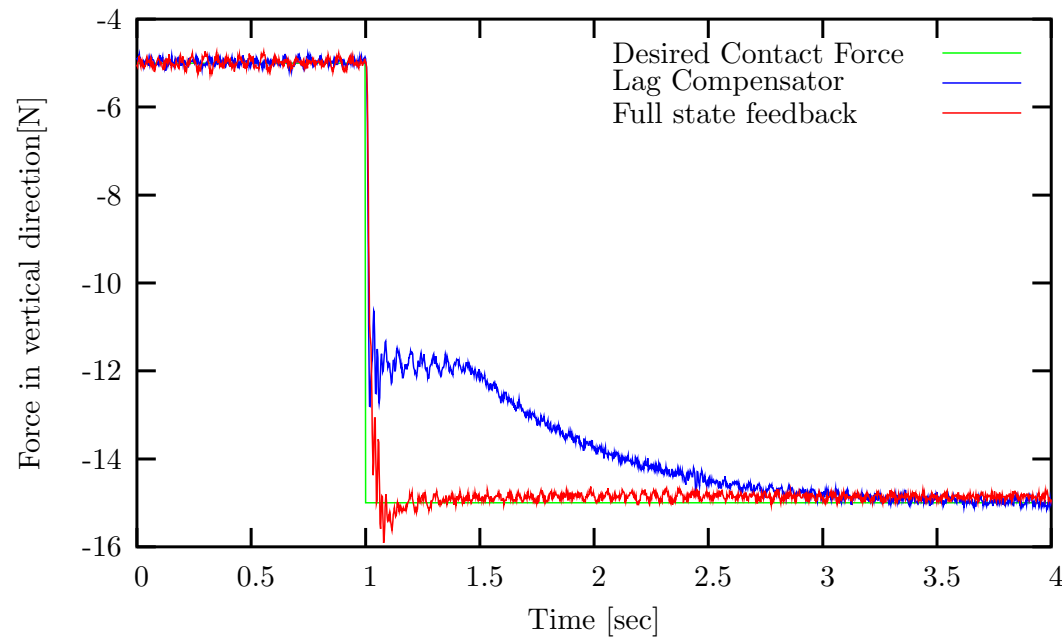
One point contact with hard surface



Full state feedback control

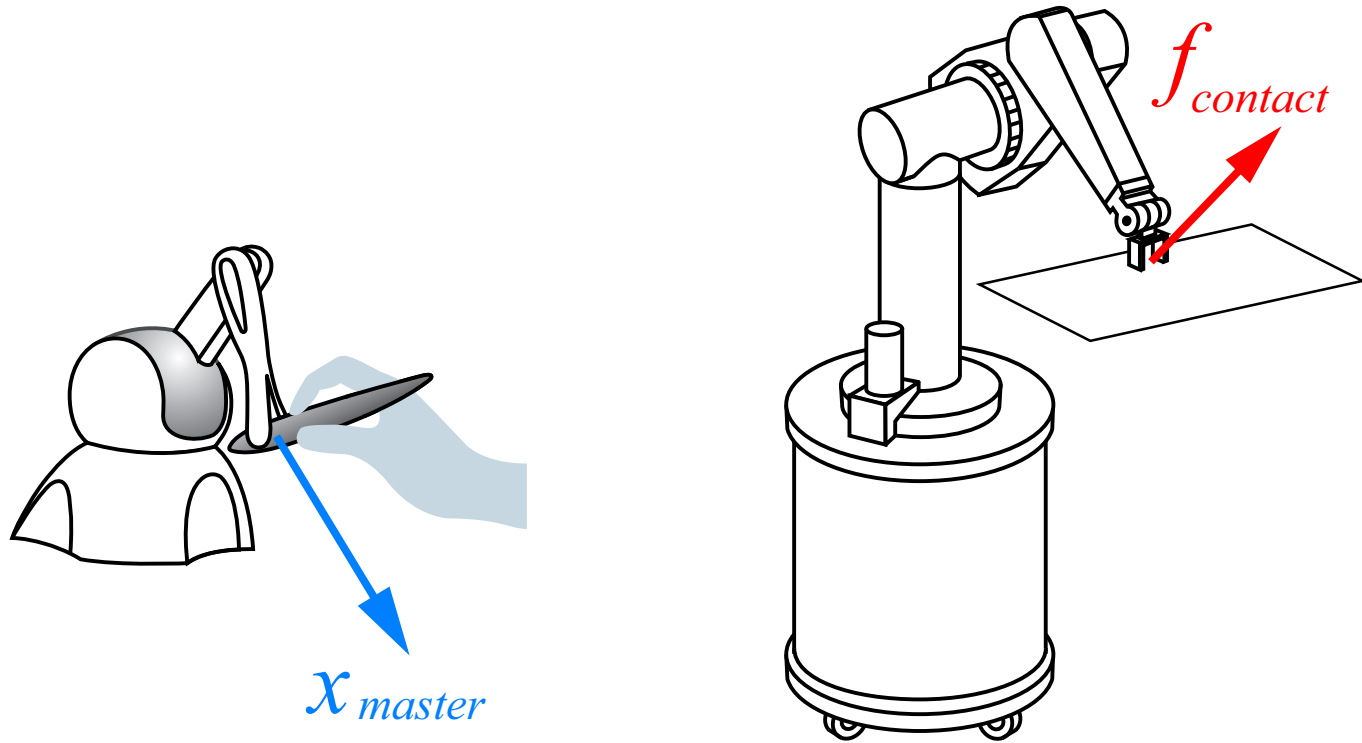
Force Control Result

One point contact with hard surface

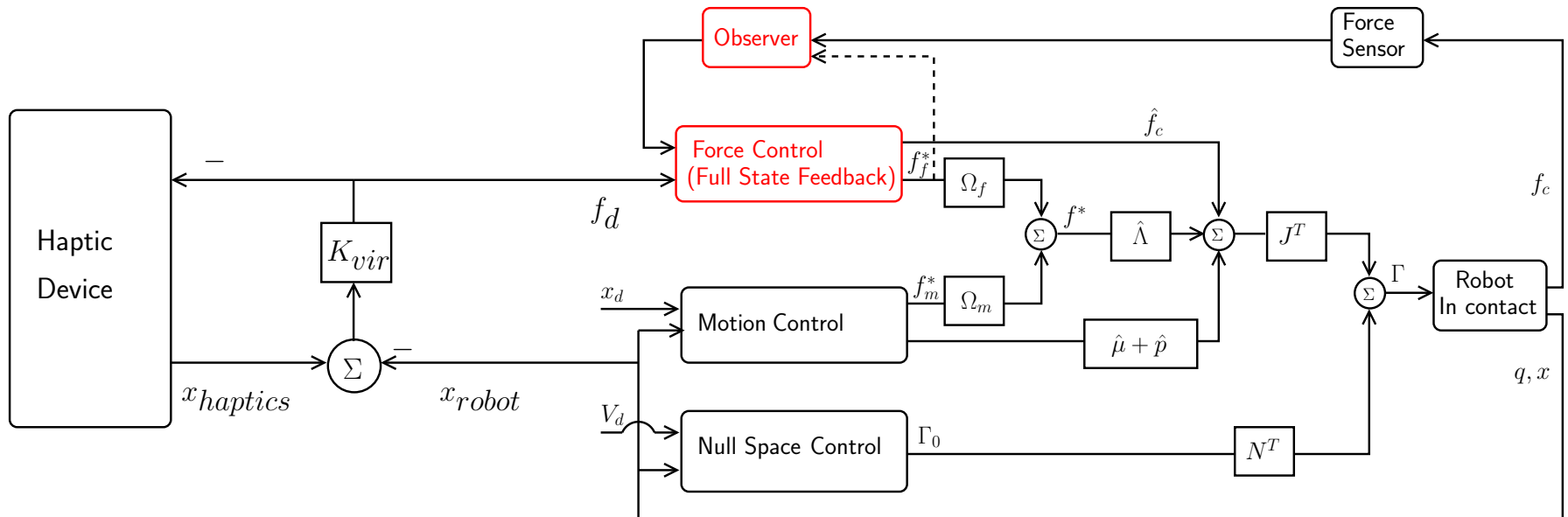


Comparison

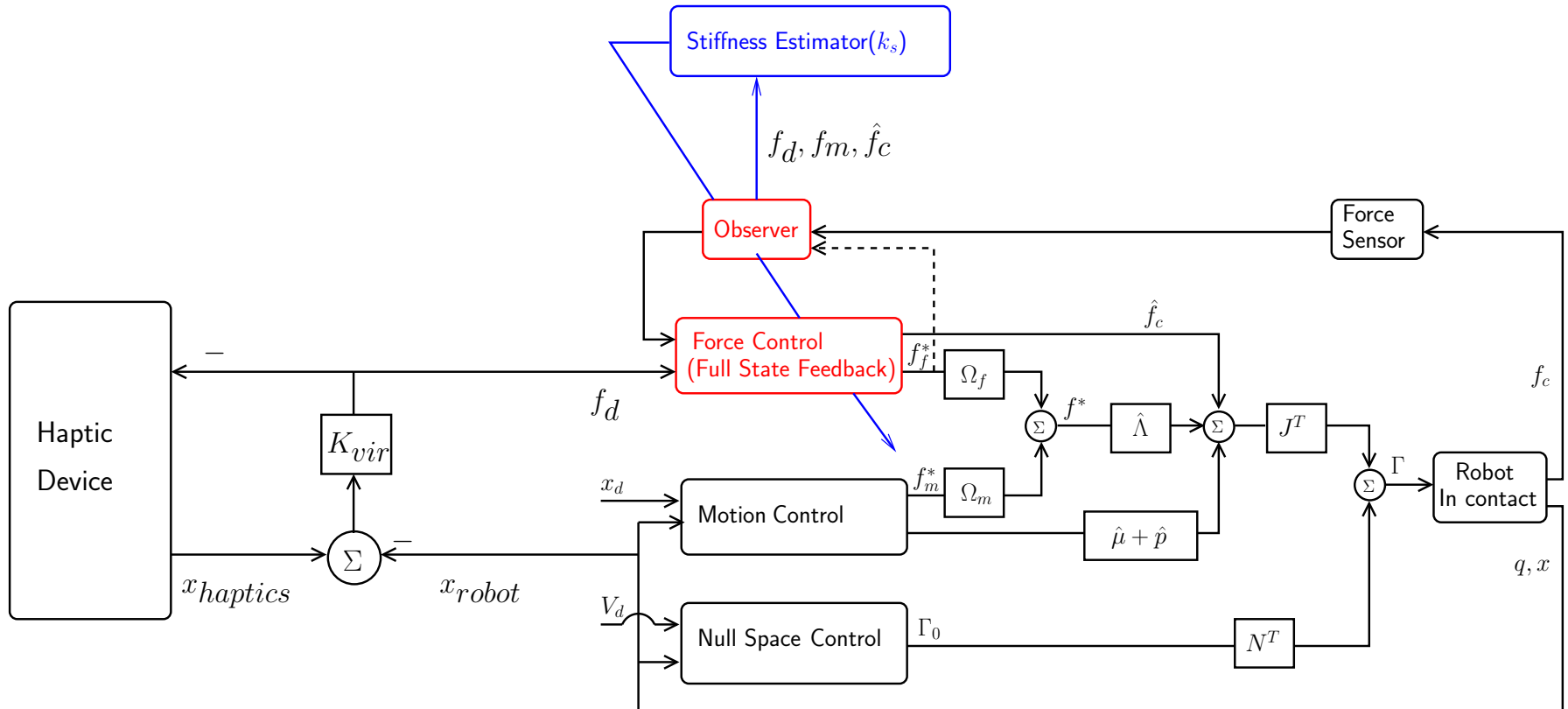
Teleoperation



Teleoperation Scheme



Teleoperation Scheme



System Setup

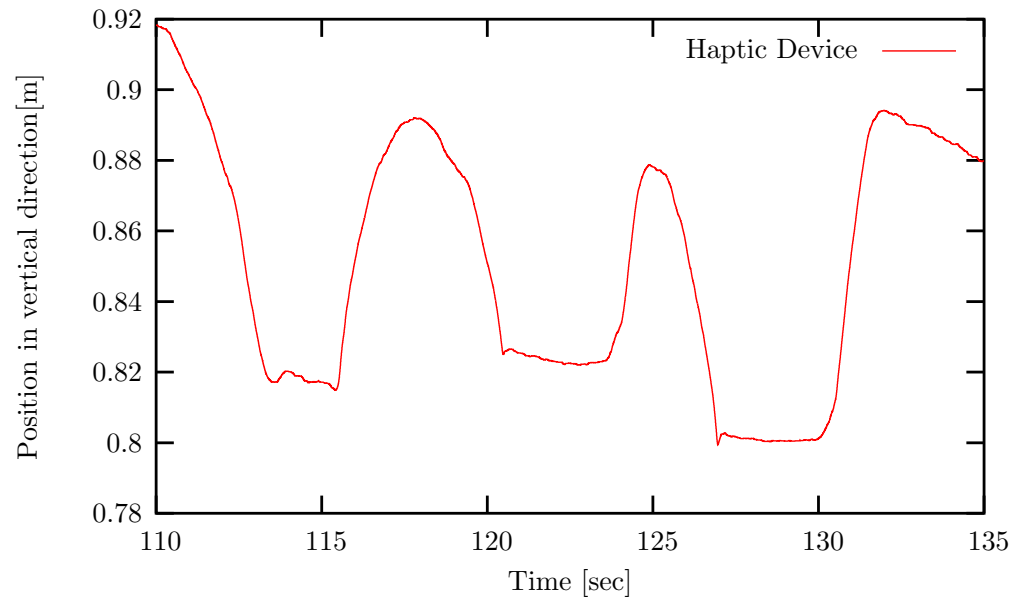


- Master Haptic Device: PHANTOM 1.0 SensAble
- Stanford Mobile Platform: PUMA560 on XR4000

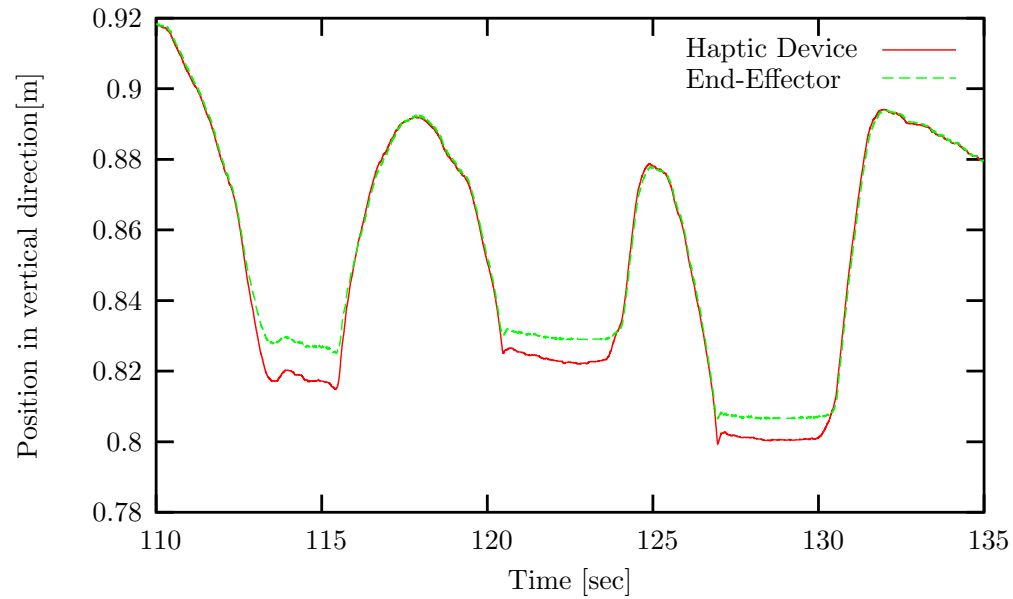
Experimental Results

- End-effector controlled by teleoperation
- Base motion is controlled in the null-space

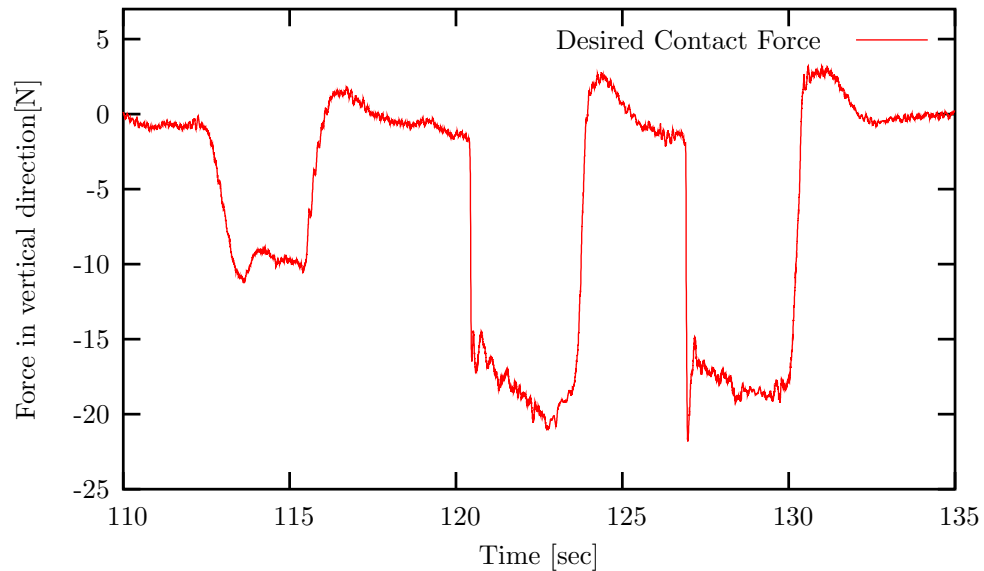
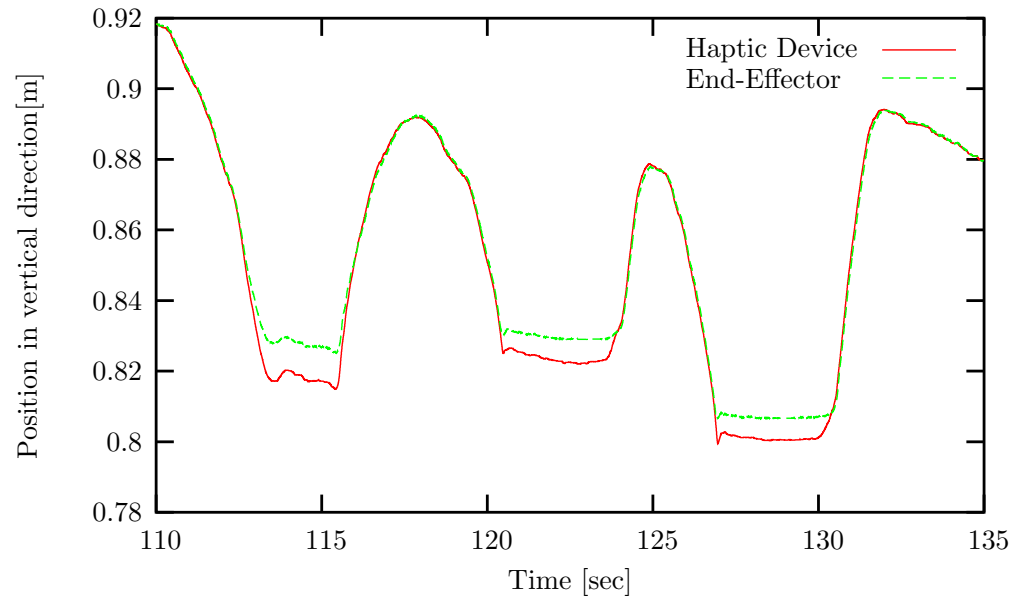
Motion/Force Tracking



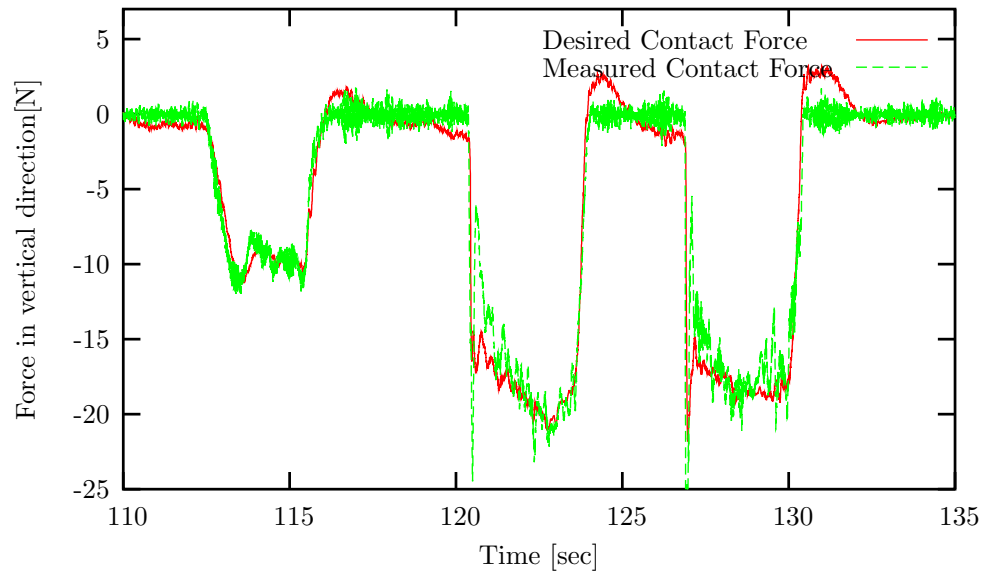
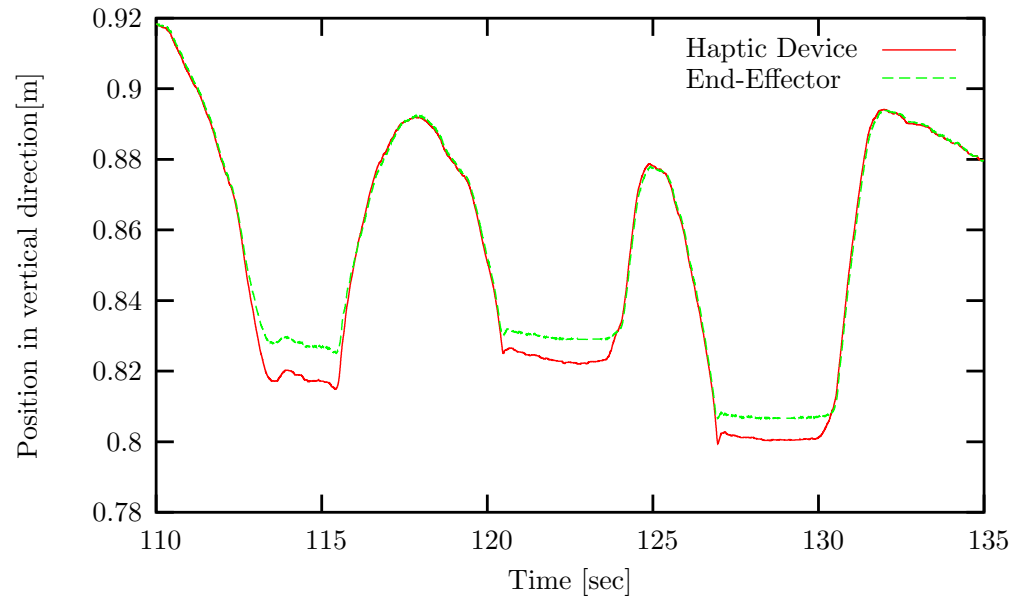
Motion/Force Tracking



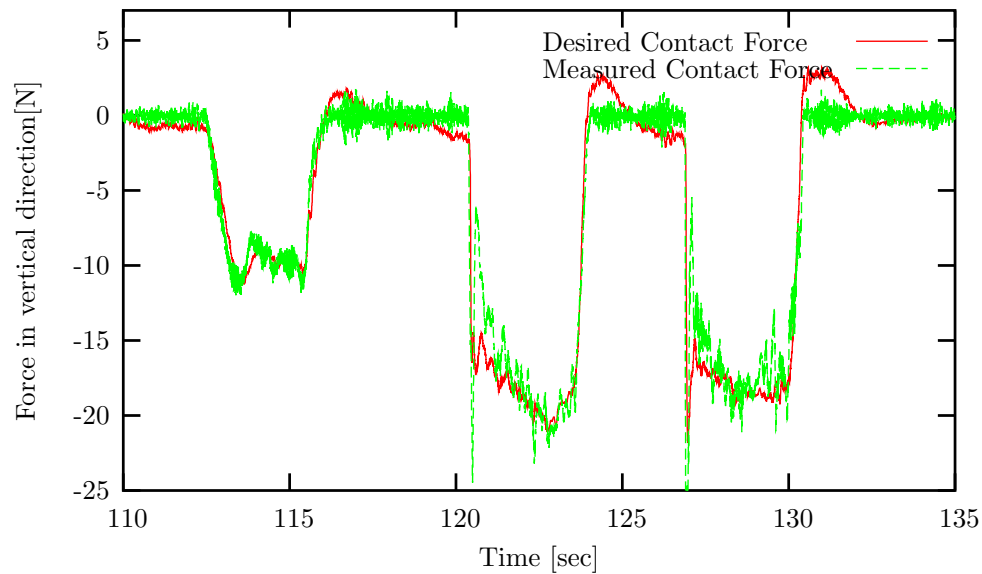
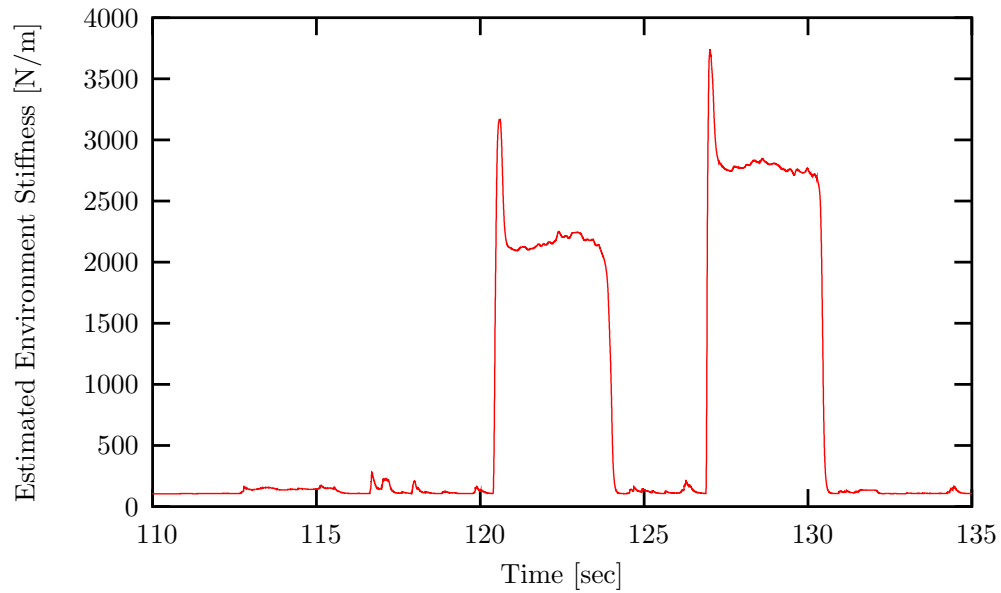
Motion/Force Tracking



Motion/Force Tracking

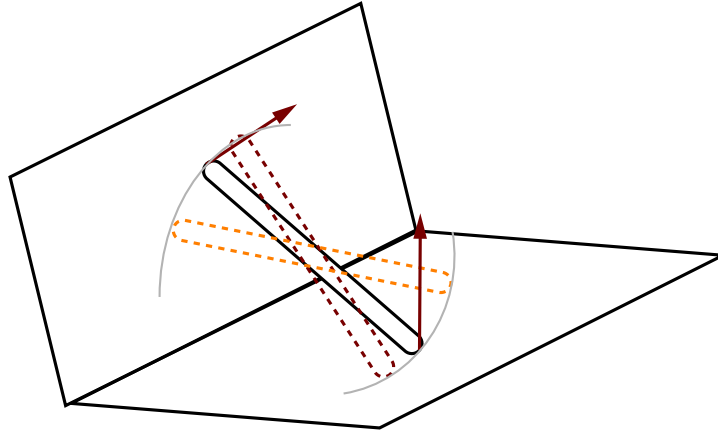


Motion/Force Tracking



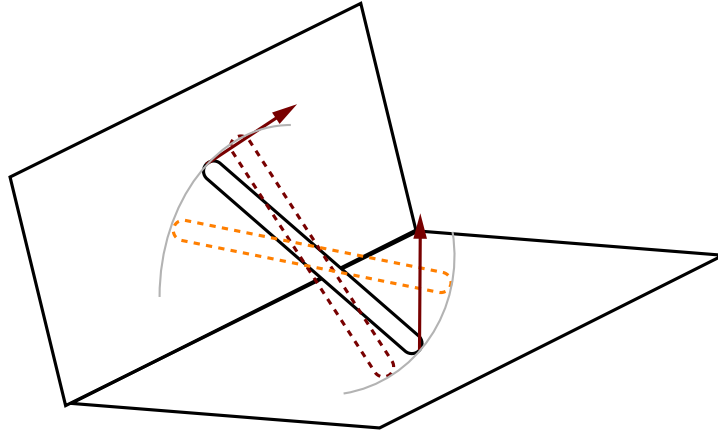
Juliet Setting a Dinner Table

Multiple Contacts



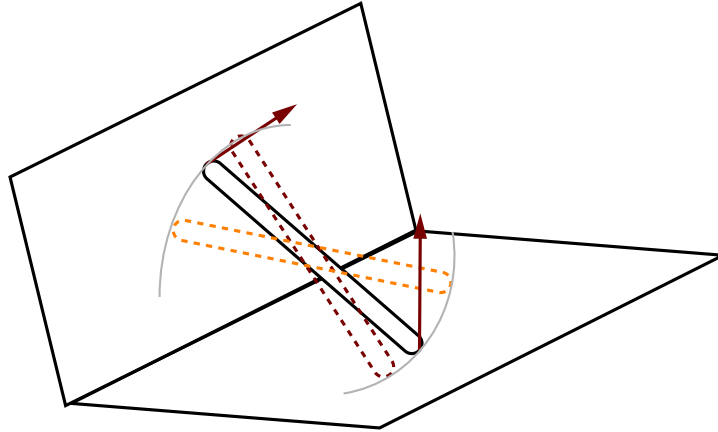
- Compliant frame selection matrices is not general enough to describe multi-contact

Multiple Contacts



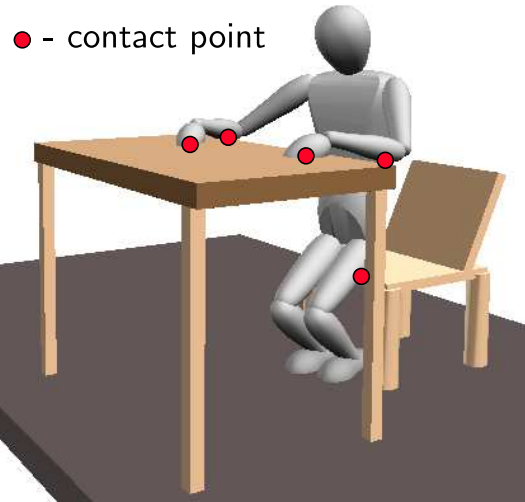
- Compliant frame selection matrices is not general enough to describe multi-contact
- Special selection matrix $\Omega_f(n)$ and $\Omega_m(n)$
 - Featherstone, Sonck, and Khatib (1997)

Multiple Contacts



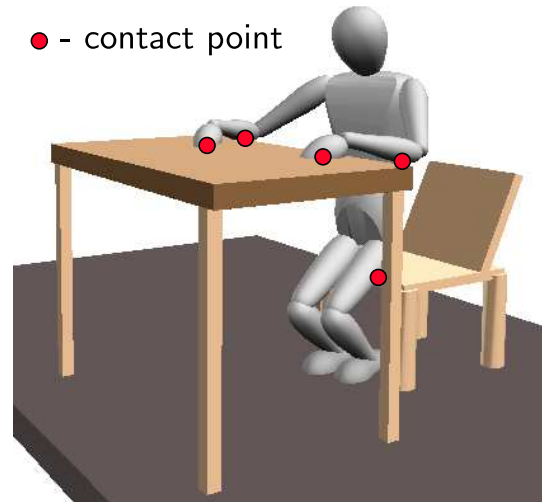
- Compliant frame selection matrices is not general enough to describe multi-contact
- Special selection matrix $\Omega_f(n)$ and $\Omega_m(n)$
 - Featherstone, Sonck, and Khatib (1997)
 - Bruyninckx and Schutter (1998)

Multi-link Multi-contact



$$\begin{pmatrix} \Lambda_{11} & \Lambda_{12} & \dots & \Lambda_{1m} \\ \Lambda_{21} & \Lambda_{22} & \dots & \Lambda_{2m} \\ \vdots & \vdots & \ddots & \vdots \\ \Lambda_{m1} & \Lambda_{m2} & \dots & \Lambda_{mm} \end{pmatrix} \begin{pmatrix} \ddot{x}_1 \\ \ddot{x}_2 \\ \vdots \\ \ddot{x}_m \end{pmatrix} + \mu + p + f_c = \begin{pmatrix} F_1 \\ F_2 \\ \vdots \\ F_m \end{pmatrix}$$

Multi-link Multi-contact

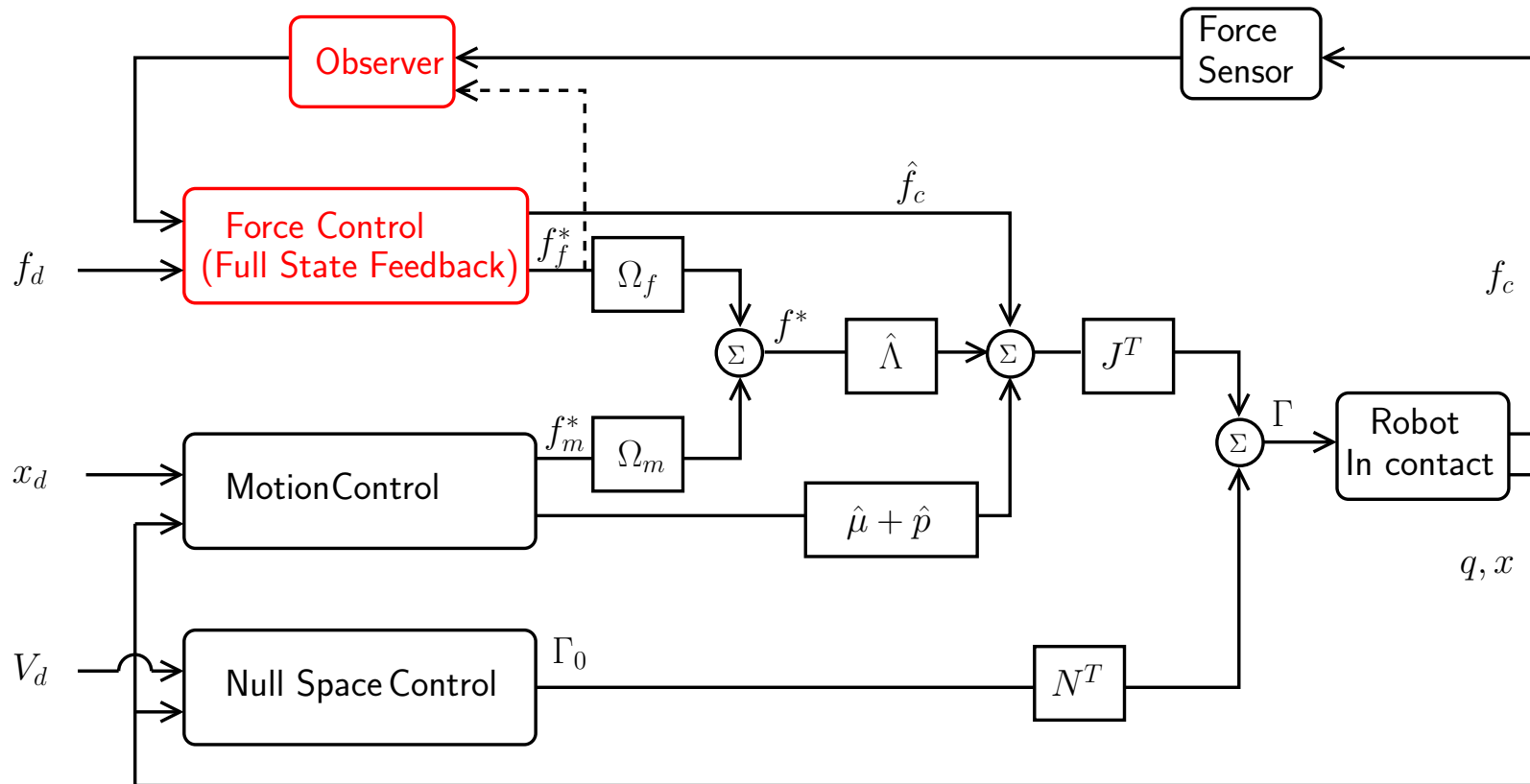


The spacial selection matrices will be defined by the contact normal directions of all the operational points : $\Omega_f(n_1, n_2, \dots, n_l)$ and $\Omega_m(n_1, n_2, \dots, n_l)$

$$F = \hat{\Lambda} f^* + \hat{\mu} + \hat{p} + \hat{f}_c$$

$$f^* = \Omega_f f_f^* + \Omega_m f_m^*$$

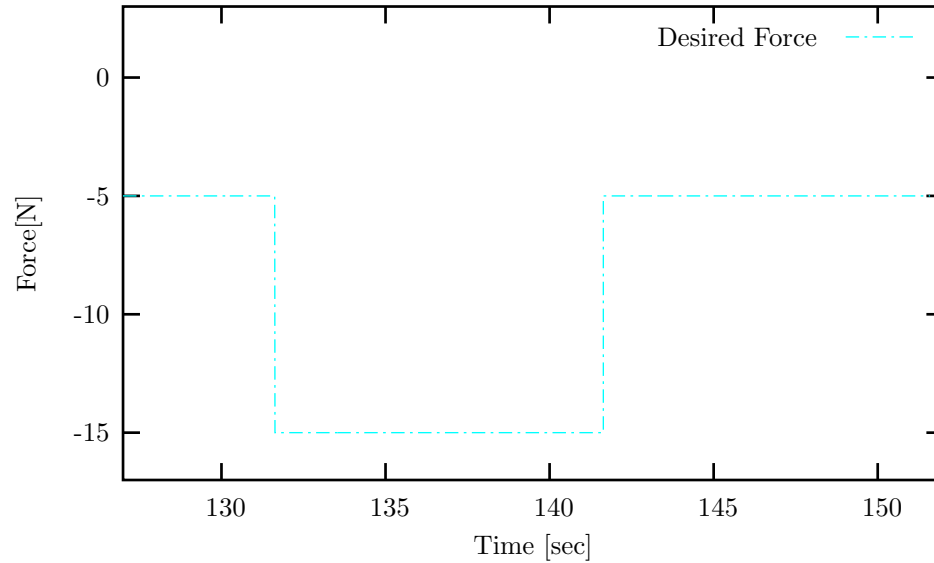
Motion/Force Control Framework



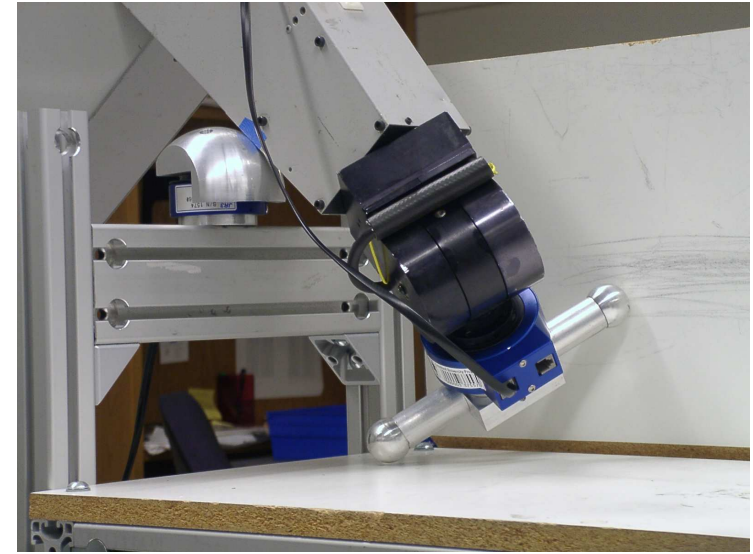
$$\begin{cases} \ddot{x}_m &= f_m^* \\ \frac{1}{k_s} \ddot{f}_c &= f_f^* \end{cases}$$

Three contact experiment

Two contact at the end-effector and one contact at the third link

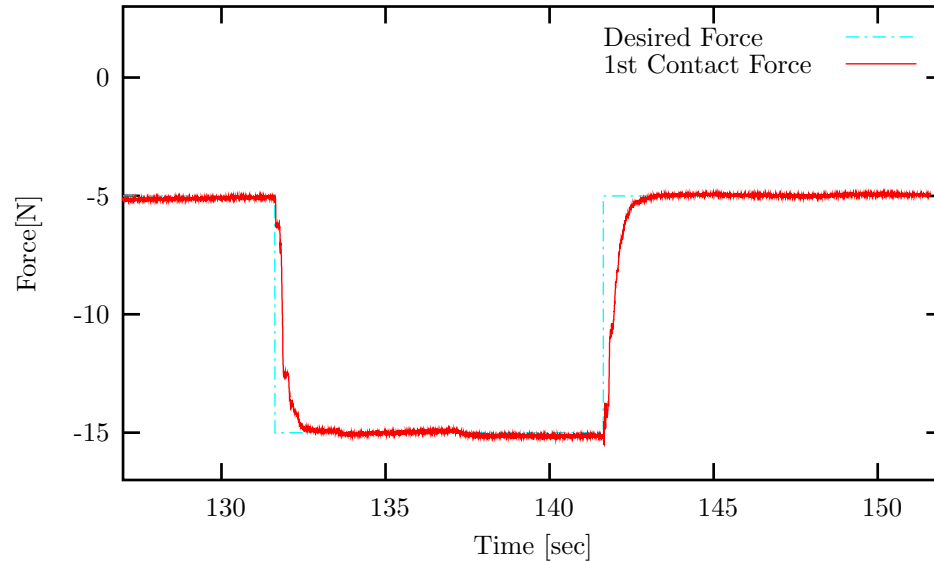


Contact force measurement

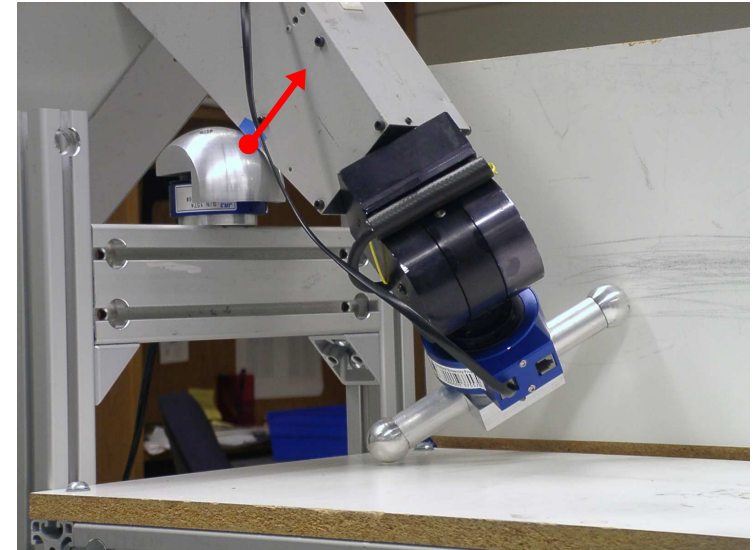


Three contact experiment

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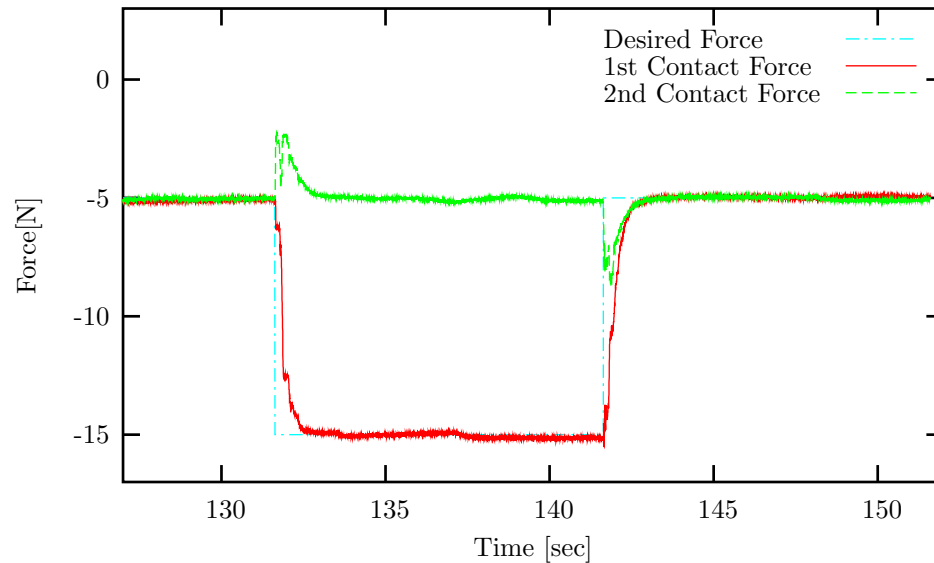


Contact force measurement

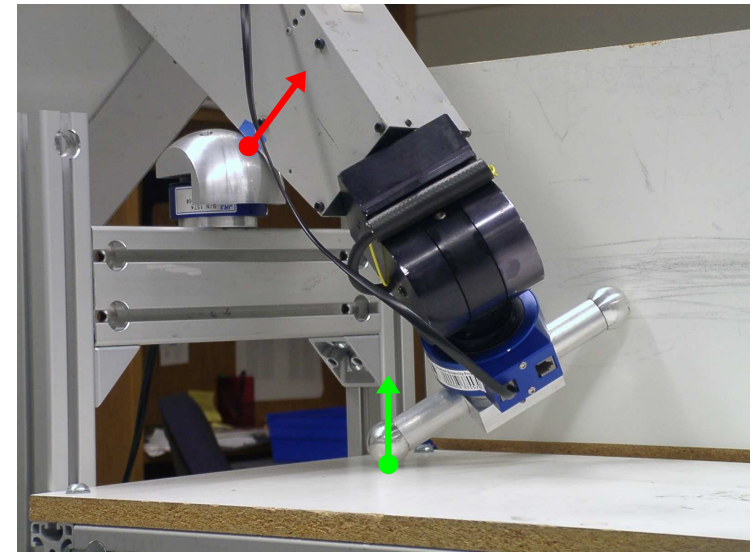


Three contact experiment

Two contact at the end-effector and one contact at the third link

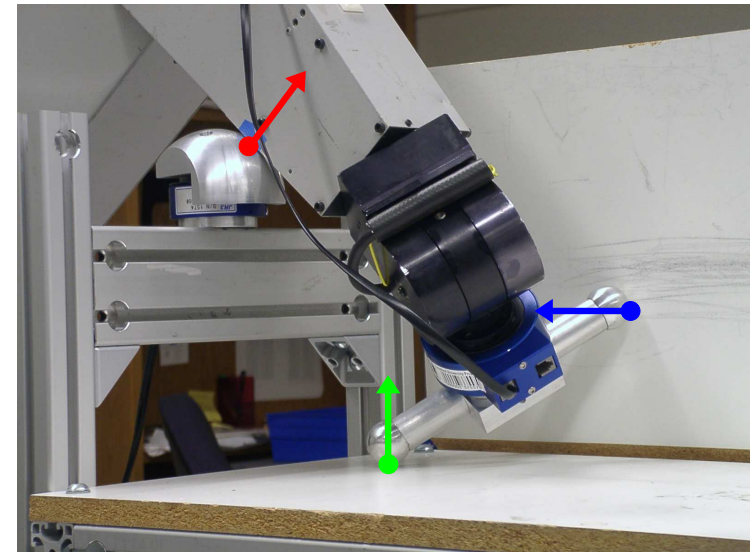
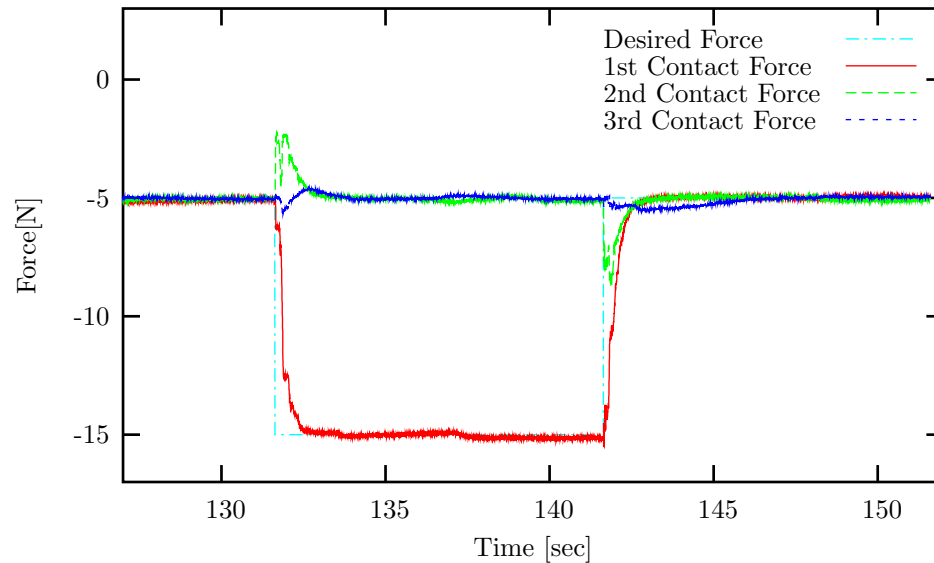


Contact force measurement



Three contact experiment

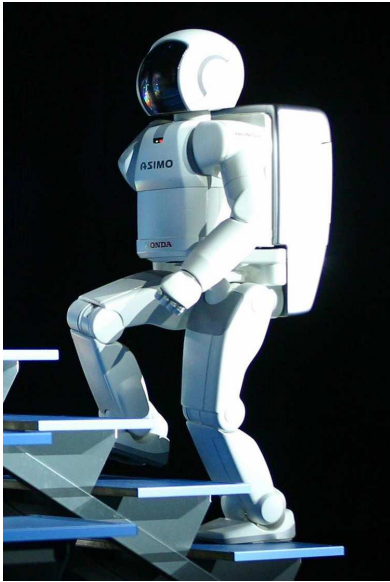
Two contact at the end-effector and one contact at the third link



Contact force measurement

Three contact experiment with motion

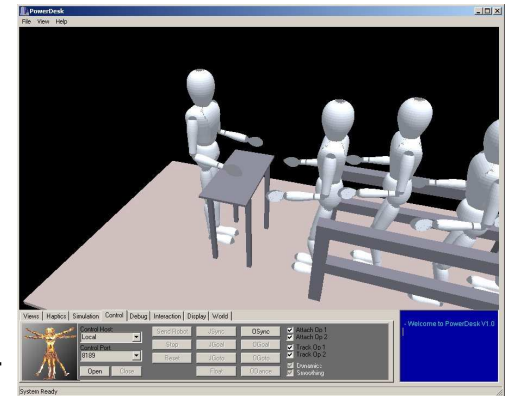
Humanoid robot



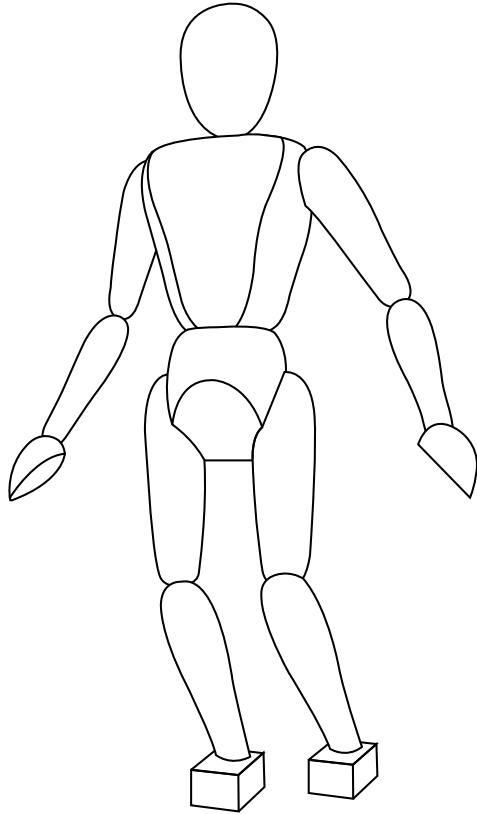
- Many humanoid systems have been built.
Honda ASIMO, Sony SDR, HRP, and KHR
- Controls are still limited
 - mostly focused on walking
 - walking and manipulation are treated as separate problems

Humanoid Research in the group

- Whole-body control framework
 - Whole-body dynamic behavior and control of human-like robots
(Khatib, Sentis, Park, Warren 2004)
- SAI simulation environment
 - Dynamic simulation
 - Efficient recursive algorithm for the operational space inertia matrix of branching mechanisms (Chang, Khatib 2001)
 - A framework for multi-contact multi-body dynamic simulation and Haptic Display (Ruspini, Khatib 2000)
 - SAI graphics engine and programming environment - Conti, Pashchenko
- Learning from human motion
 - Simulating the Task-level Control of Human Motion: A Methodology and Framework for Implementation
(De Sapia, Warren, Khatib, and Delp 2005)
- Control implementation on ASIMO - Thaulad

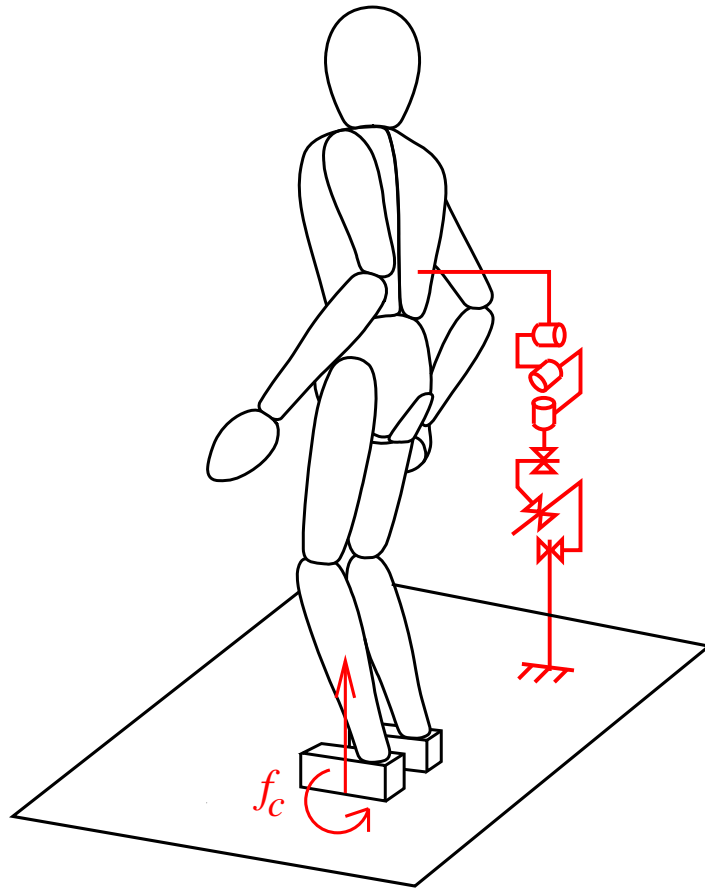


Humanoid robot characteristics



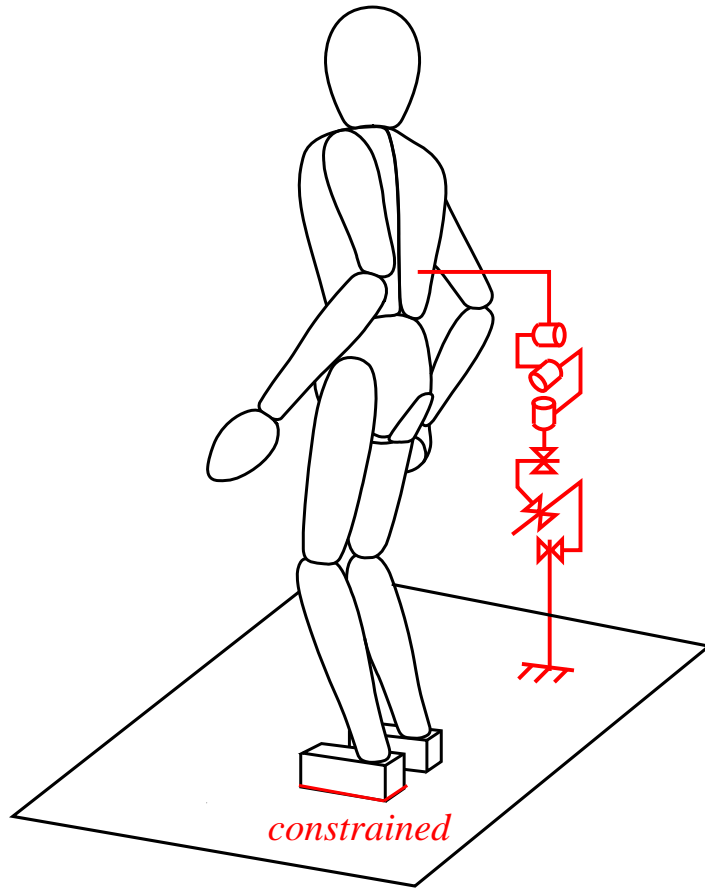
- Under-actuated system in free space
- Non fixed base
- Contacts are necessary to support the system

Constrained dynamics of robot



$$A(q)\ddot{q} + b(q, \dot{q}) + g(q) + J_c^T \textcircled{f_c} = \Gamma$$

Constrained dynamics of robot

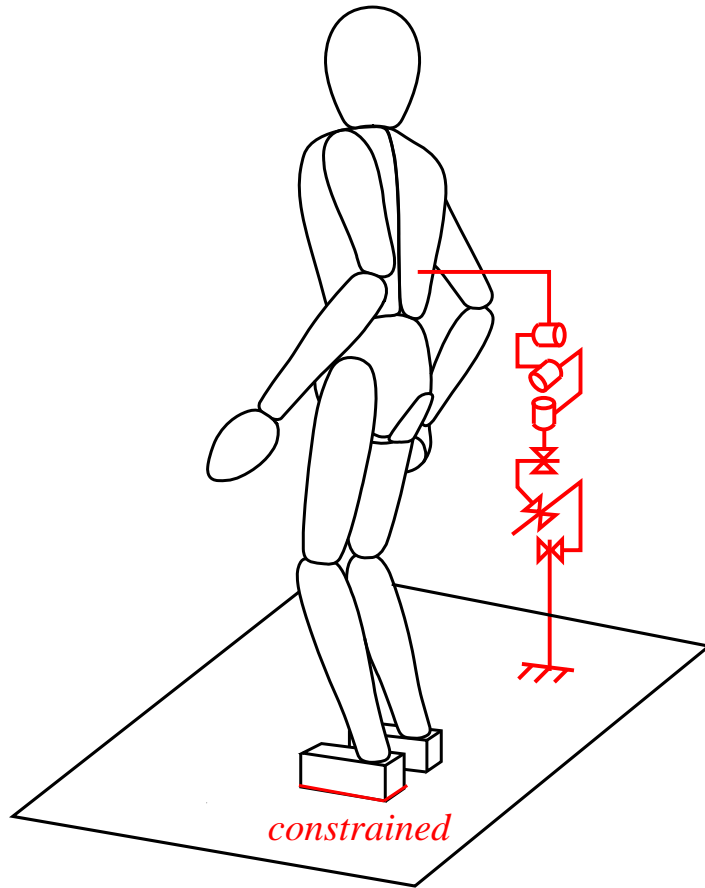


$$A(q)\ddot{q} + b(q, \dot{q}) + g(q) + J_c^T \textcircled{f_c} = \Gamma$$

By treating the contacts as constraints, $\ddot{x}_c = 0$ and $\dot{x}_c = 0$,

$$\textcircled{f_c} = \bar{J}_c^T(q)\Gamma - \mu_c(q, \dot{q}) - p_c(q)$$

Constrained dynamics of robot



$$A(q)\ddot{q} + b(q, \dot{q}) + g(q) + J_c^T \textcircled{f_c} = \Gamma$$

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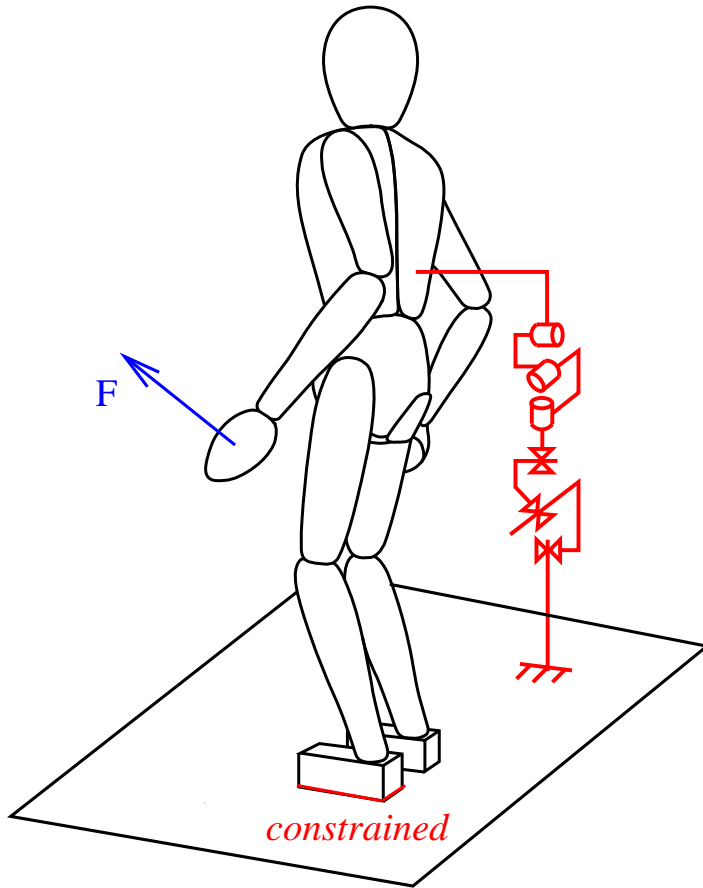
$$\textcircled{f_c} = \bar{J}_c^T(q)\Gamma - \mu_c(q, \dot{q}) - p_c(q)$$

$$\begin{aligned} \Rightarrow A(q)\ddot{q} + b(q, \dot{q}) + g(q) \\ - J_c^T (\mu_c(q, \dot{q}) + p_c(q)) \\ = (I - J_c^T \bar{J}_c^T)\Gamma \end{aligned}$$

Operational Space Dynamics

Constrained Joint Space Dynamics

$$\begin{aligned} A\ddot{q} + b + g - J_c^T(\mu_c + p_c) \\ = (I - J_c^T \bar{J}_c^T)\Gamma \end{aligned}$$



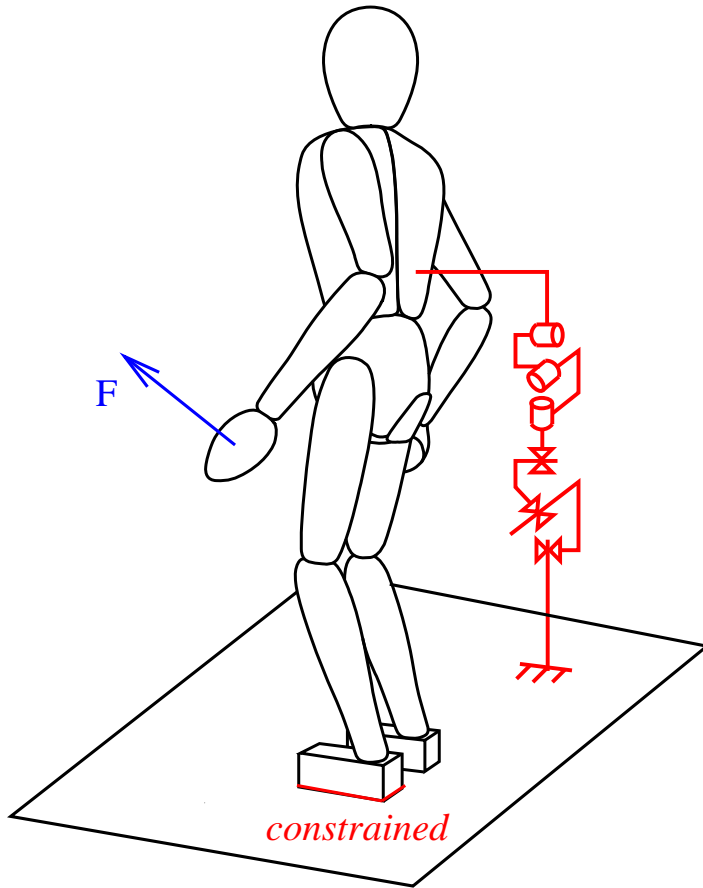
Operational Space Dynamics

Constrained Joint Space Dynamics

$$A\ddot{q} + b + g - J_c^T(\mu_c + p_c) \\ = (I - J_c^T \bar{J}_c^T)\Gamma$$

Constrained Operational space dynamics

$$\Lambda\ddot{x} + \mu(q, \dot{q}) + p(q) = F$$



Operational Space Dynamics

Constrained Joint Space Dynamics

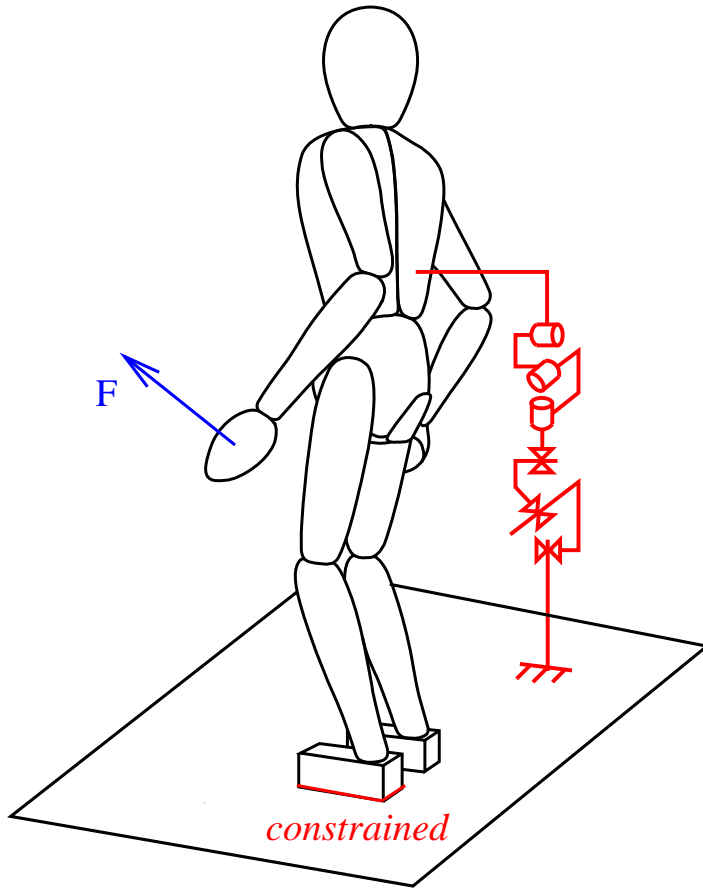
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Constrained Operational space dynamics

$$\Lambda\ddot{x} + \mu(q, \dot{q}) + p(q) = F$$

Control Force

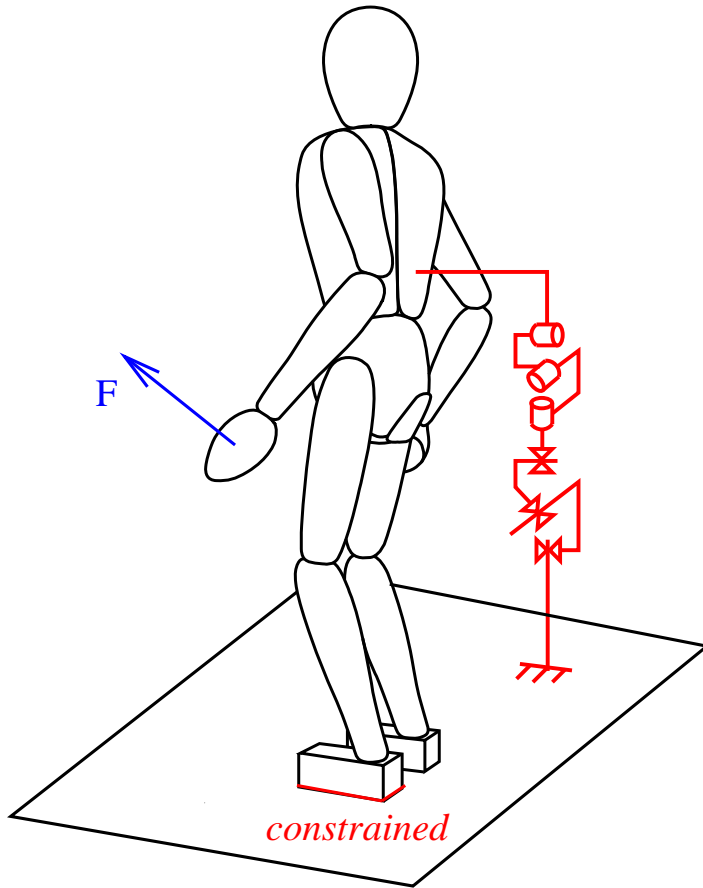
$$F = \hat{\Lambda}f^* + \hat{\mu} + \hat{p}$$



Control Torque

The relation between joint torque and force

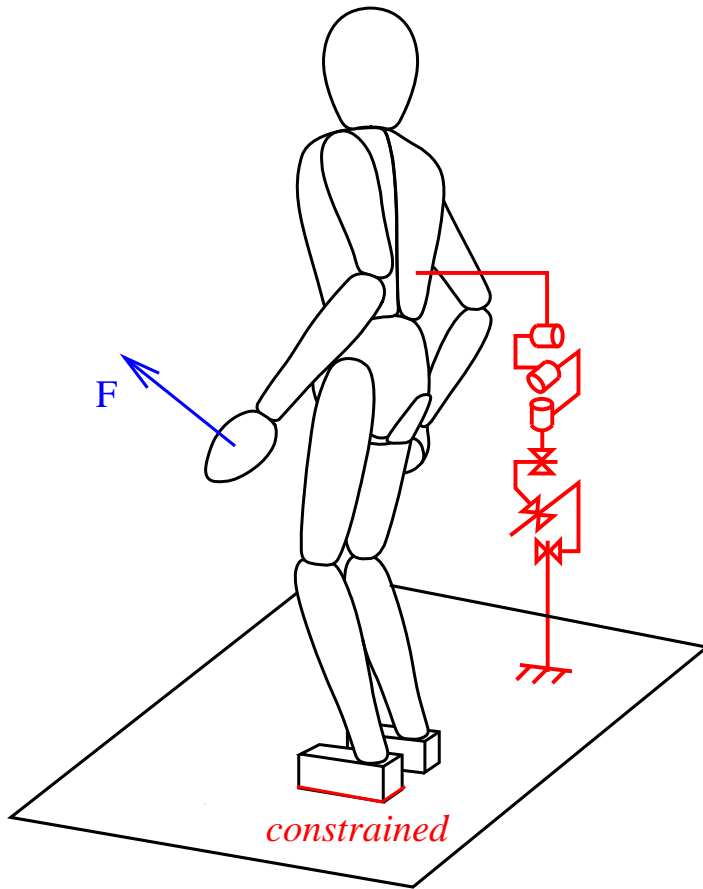
$$\Gamma = J^T F$$



Control Torque

The relation between joint torque and force

$$F = \bar{J}^T \Gamma$$



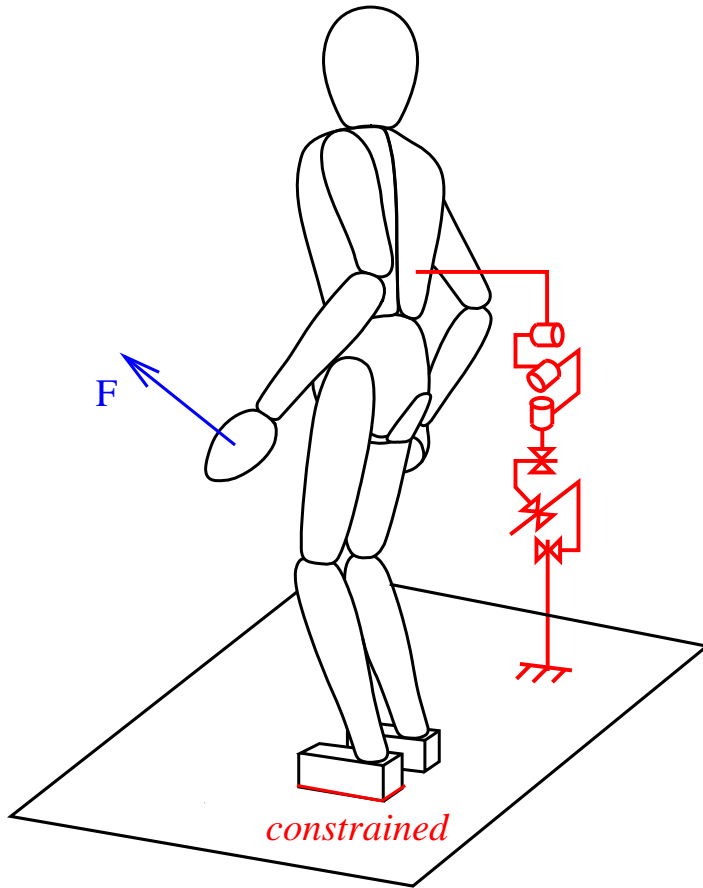
Control Torque

The relation between joint torque and force

$$F = \bar{J}^T \Gamma$$

Torques at virtual joints are zero.

$$F = \bar{J}^T S^T \Gamma_{actuated}$$



Control Torque

The relation between joint torque and force

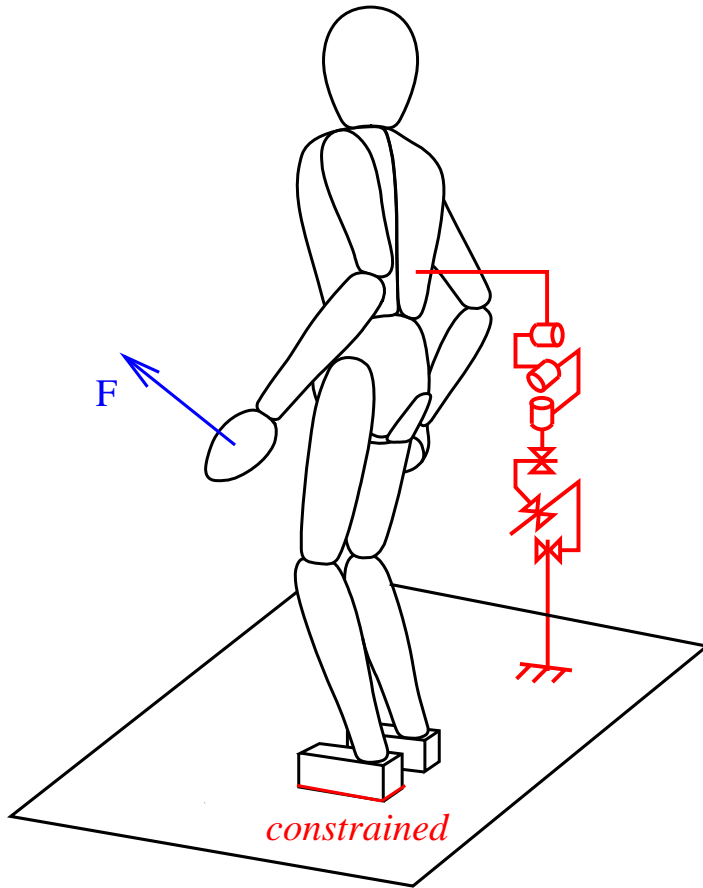
$$F = \bar{J}^T \Gamma$$

Torques at virtual joints are zero.

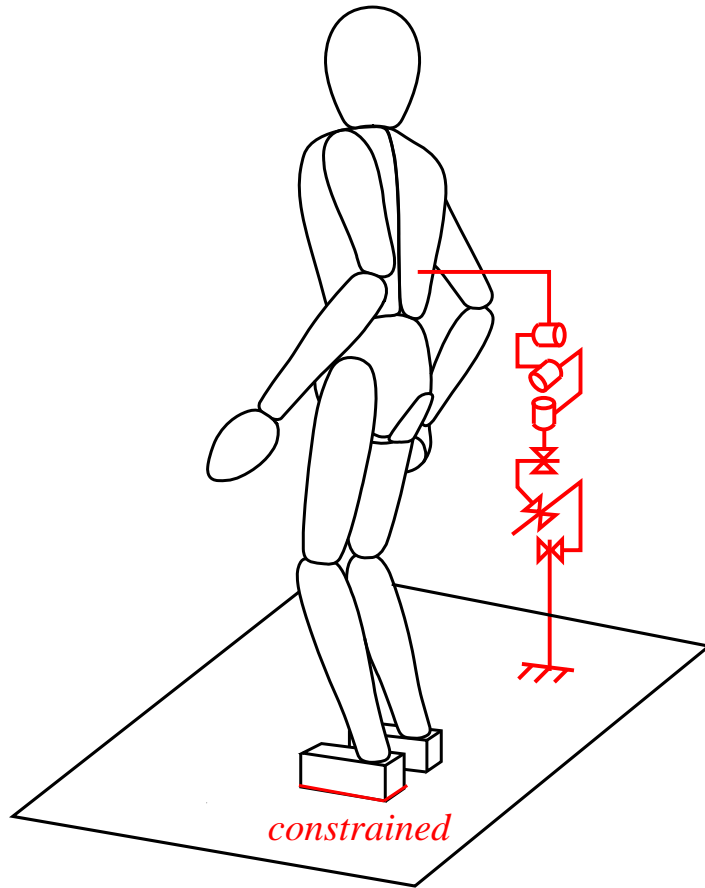
$$F = \bar{J}^T S^T \Gamma_{actuated}$$

The Control torque is

$$(\Gamma_{actuated})_{task} = \overline{\bar{J}^T S^T} F$$



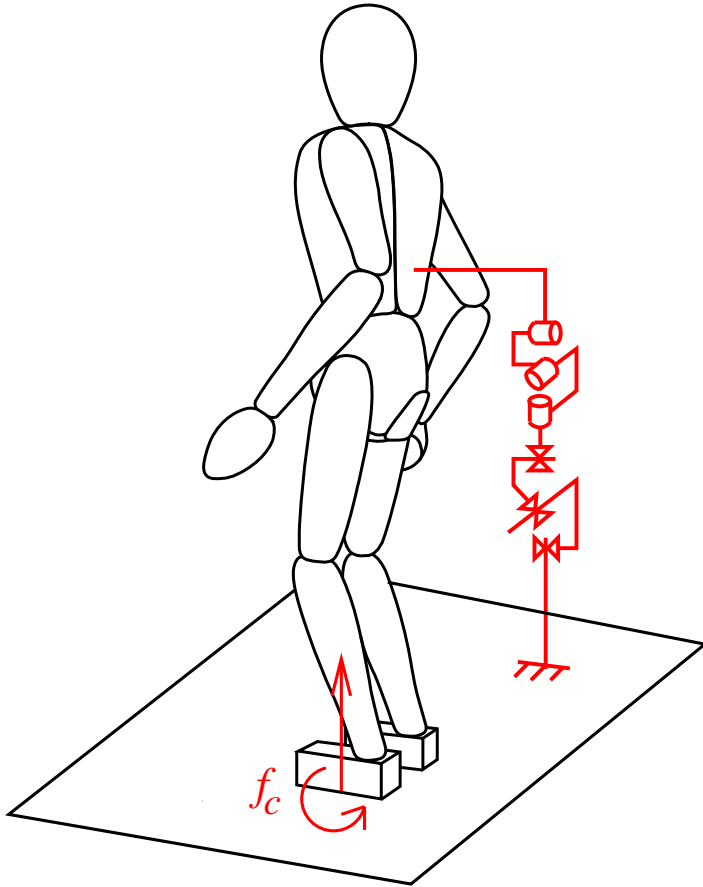
Constrained dynamics of robot



$$A\ddot{q} + b + g - J_c^T(\mu_c + p_c) \\ = (I - J_c^T \bar{J}_c^T)\Gamma$$

$$f_c = \bar{J}_c^T \Gamma - \mu_c(q, \dot{q}) - p_c(q)$$

Constrained dynamics of robot



$$A\ddot{q} + b + g - J_c^T(\mu_c + p_c) \\ = (I - J_c^T \bar{J}_c^T) \Gamma$$

$$f_c = \bar{J}_c^T \Gamma - \mu_c(q, \dot{q}) - p_c(q)$$

$$f_{c,i}|_{min} < f_{c,i} < f_{c,i}|_{max}$$

Reaction Force Control

$$\Gamma_{actuated} = (\Gamma_{actuated})_{task}$$

Reaction forces are given by

$$f_c = \bar{J}_c^T S^T (\Gamma_{actuated})_{task} - \mu_c(q, \dot{q}) - p_c(q)$$

Reaction Force Control

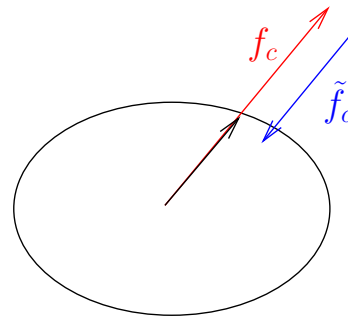
$$\Gamma_{actuated} = (\Gamma_{actuated})_{task} + (\Gamma_{actuated})_{contact}$$

Reaction forces are given by

$$f_c = \bar{J}_c^T S^T (\Gamma_{actuated})_{task} - \mu_c(q, \dot{q}) - p_c(q)$$

Modify control torque if they exceed the boundaries,

$$(\Gamma_{actuated})_{contact} = \overline{\bar{J}_c^T S^T} \tilde{f}_c$$



Standing on two feet

Gravity compensation with reaction force control

Balancing

Controlled operational space coordinates

- Position of Center of Mass AND Orientation of head, chest, and hip

Walking

Controlled operational space coordinates

- Position of Center of Mass AND Orientation of head, chest, and hip
- Left or right foot in one foot supporting

Jumping

Controlled operational space coordinates

- Position of Center of Mass AND Orientation of head, chest, and hip
- Both feet at no contact

Climbing Ladder

Controlled operational space coordinates

- Position of Center of Mass AND Orientation of head, chest, and hip
- Hands or feet in climbing

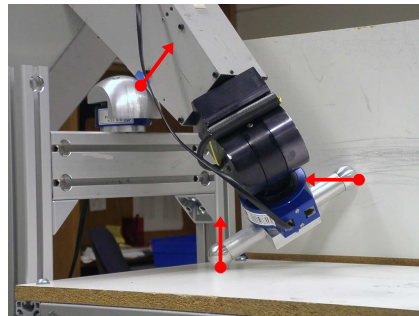
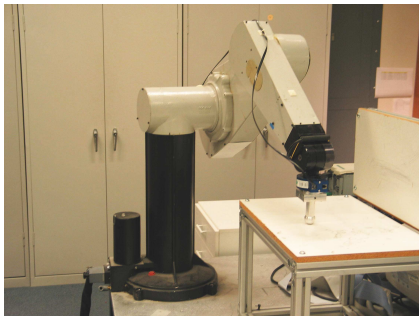
Manipulation combined with walking

Controlled operational space coordinates

- Position of Center of Mass AND Orientation of head, chest, and hip
- Position and Force control of right hand

Conclusion

- Robust force control was developed for multi-body robotic systems.
 - High performance was demonstrated using full state feedback with Kalman estimator (improvement over lag compensator).
- Haptic teleoperation was implemented.
 - High fidelity transparent teleoperation was achieved by using force control with stiffness estimation.
- Motion/force control structure was generalized.
 - Composition of decoupled motion/force control was achieved by constructing selection matrices over multiple control points.
- Contact force consistent control strategy was developed for humanoid systems
 - This enables implementation of motion/force control to non fixed base robots.



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